

CES 141

Compulsory Ethiopian Standard

First Edition
2015

Basis of Structural Design



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Foreword

This Ethiopian Standard has been prepared under the direction of the Technical Committee for Building structures and elements of building (TC 42) and published by the Ethiopian Standards Agency (ESA).

This Ethiopian standard is an adaption of EN 1990:2002, Basis of Structural Design, with permission of CEN, Avenue Marnix 17, B-1000 Brussels

In the preparation the Addis Ababa Univerisity reviewed the draft document under the supervision of Ministry of Construction.

Acknowledgment has been made for the organizations for their concern to contribute to the effort of national standardization.

Application of this standard is **COMPULSORY** with respect Section 2-6 .

A Compulsory Ethiopian Standard shall have the same meaning, interpretation and application of a "Technical Regulation" as implied in the WTO-TBT Agreement.

Implementation of this standard shall be effective as of May 01 2018.

Basis of Structural Design

SECTION 1. GENERAL

1.1 Scope

(1) ES EN 1990:2015 establishes Principles and requirements for the safety, serviceability and durability of structures, describes the basis for their design and verification and gives guidelines for related aspects of structural reliability.

(2) ES EN 1990:2015 is intended to be used in conjunction with ES EN 1991:2015 to ES EN 1998:2015 for the structural design of buildings and civil engineering works, including geotechnical aspects, structural fire design, situations involving earthquakes, execution and temporary structures.

Note: For the design of special construction works (e.g. nuclear installations, dams, etc.), other provisions than those in ES EN 1990:2015 to ES EN 1998:2015 might be necessary.

(3) ES EN 1990:2015 is applicable for the design of structures where other materials or other actions outside the scope of ES EN 1991:2015 to ES EN 1998:2015 are involved.

(4) ES EN 1990:2015 is applicable for the structural appraisal of existing construction, in developing the design of repairs and alterations or in assessing changes of use.

Note: Additional or amended provisions might be necessary where appropriate.

1.2 Normative references

This Ethiopian Standard, which is based on EN 1990, incorporates by dated or undated reference, provisions from other publications. These normative references are cited at the appropriate places in the text and the publications are listed hereafter. For dated references, subsequent amendments to or revisions of any of these publications apply to this Ethiopian Standard only when incorporated in it by amendment or revision. For undated references the latest edition of the publication referred to applies (including amendments).

Note: The following Ethiopian Standards which are published are cited in normative clauses:

ES EN 1991:2015 ES 1: Actions on structures

ES EN 1992:2015 ES 2: Design of concrete structures

ES EN 1993:2015 ES 3: Design of steel structures

ES EN 1994:2015 ES 4: Design of composite steel and concrete structures

ES EN 1995:2015 ES 5: Design of timber structures

ES EN 1996:2015 ES 6: Design of masonry structures

ES EN 1997:2015 ES 7: Geotechnical design

ES EN 1998:2015 ES 8: Design of structures for earthquake resistance

1.3 Assumptions

(1) Design which employs the Principles and Application Rules is deemed to meet the requirements provided the assumptions given in ES EN 1990:2015 to ES EN 1998:2015 are satisfied (see Section 2).

(2) The general assumptions of ES EN 1990:2015 are:

- the choice of the structural system and the design of the structure is made by appropriately qualified and experienced personnel;
- execution is carried out by personnel having the appropriate skill and experience;
- adequate supervision and quality control is provided during execution of the work, i.e. in design offices, factories, plants, and on site;
- the construction materials and products are used as specified in ES EN 1990:2015 or in ES EN 1991:2015 to ES EN 1998:2015 or in the relevant execution standards, or reference material or product specifications;
- the structure will be adequately maintained;
- the structure will be used in accordance with the design assumptions.

Note: There may be cases when the above assumptions need to be supplemented.

1.4 Distinction between Principles and Application Rules

(1) Depending on the character of the individual clauses, distinction is made in ES EN 1990:2015 between Principles and Application Rules.

(2) The Principles comprise:

- general statements and definitions for which there is no alternative, as well as ;
- requirements and analytical models for which no alternative is permitted unless specifically stated.

(3) The Principles are identified by the letter P following the paragraph number.

(4) The Application Rules are generally recognised rules which comply with the Principles and satisfy their requirements.

(5) It is permissible to use alternative design rules different from the Application Rules given in ES EN 1990:2015 for works, provided that it is shown that the alternative rules accord with the relevant Principles and are at least equivalent with regard to the structural safety, serviceability and durability which would be expected when using the ES.

Note: If an alternative design rule is substituted for an application rule, the resulting design cannot be claimed to be wholly in accordance with ES EN 1990:2015 although the design will remain in accordance with the Principles of ES EN 1990:2015.

(6) In ES EN 1990:2015, the Application Rules are identified by a number in brackets e.g. as this clause.

1.5 Terms and definitions

Note: For the purposes of this Ethiopian Standard, the Terms and definitions are derived from ES ISO 2394, ES ISO 3898, ES ISO 8930, ES ISO 8402.

1.5.1 Common terms used in ES EN 1990:2015 to ES EN 1998:2015

1.5.1.1

construction works

everything that is constructed or results from construction operations

Note: This definition accords with ES ISO 6707-1. The term covers both building and civil engineering works. It refers to the complete construction works comprising structural, non-structural and geotechnical elements.

1.5.1.2

type of building or civil engineering works

type of construction works designating its intended purpose, *e.g.* dwelling house, retaining wall, industrial building, road bridge

1.5.1.3

type of construction

indication of the principal structural material, *e.g.* reinforced concrete construction, steel construction, timber construction, masonry construction, steel and concrete composite construction.

1.5.1.4

method of construction

manner in which the execution will be carried out, *e.g.* cast in place, prefabricated, cantilevered

1.5.1.5

construction material

material used in construction work, *e.g.* concrete, steel, timber, masonry

1.5.1.6

structure

organised combination of connected parts designed to carry loads and provide adequate rigidity

1.5.1.7

structural member

physically distinguishable part of a structure, *e.g.* a column, a beam, a slab, a foundation pile

1.5.1.8

form of structure

arrangement of structural members

Note: Forms of structure are, for example, frames, suspension bridges.

1.5.1.9

structural system

load-bearing members of a building or civil engineering works and the way in which these members function together

1.5.1.10

structural model

idealisation of the structural system used for the purposes of analysis, design and verification

1.5.1.11

execution

all activities carried out for the physical completion of the work including procurement, the inspection and documentation thereof

Note: The term covers work on site; it may also signify the fabrication of components off site and their subsequent erection on site.

1.5.2 Special terms relating to design in general

1.5.2.1

design criteria

quantitative formulations that describe for each limit state the conditions to be fulfilled

1.5.2.2

design situations

sets of physical conditions representing the real conditions occurring during a certain time interval for which the design will demonstrate that relevant limit states are not exceeded

1.5.2.3

transient design situation

design situation that is relevant during a period much shorter than the design working life of the structure and which has a high probability of occurrence

Note: A transient design situation refers to temporary conditions of the structure, of use, or exposure, e.g. during construction or repair.

1.5.2.4

persistent design situation

design situation that is relevant during a period of the same order as the design working life of the structure

Note: Generally it refers to conditions of normal use.

1.5.2.5

accidental design situation

design situation involving exceptional conditions of the structure or its exposure, including fire, explosion, impact or local failure

1.5.2.6

fire design

design of a structure to fulfill the required performance in case of fire

1.5.2.7**seismic design situation**

design situation involving exceptional conditions of the structure when subjected to a seismic event

1.5.2.8**design working life**

assumed period for which a structure or part of it is to be used for its intended purpose with anticipated maintenance but without major repair being necessary.

1.5.2.9**hazard**

for the purpose of ES EN 1990:2015 to ES EN 1998:2015, an unusual and severe event, e.g. an abnormal action or environmental influence, insufficient strength or resistance, or excessive deviation from intended dimensions

1.5.2.10**load arrangement**

identification of the position, magnitude and direction of a free action

1.5.2.11**load case**

compatible load arrangements, sets of deformations and imperfections considered simultaneously with fixed variable actions and permanent actions for a particular verification

1.5.2.12**limit states**

states beyond which the structure no longer fulfills the relevant design criteria

1.5.2.13**ultimate limit states**

states associated with collapse or with other similar forms of structural failure

Note: They generally correspond to the maximum load-carrying resistance of a structure or structural member.

1.5.2.14**serviceability limit states**

states that correspond to conditions beyond which specified service requirements for a structure or structural member are no longer met

irreversible serviceability limit states

serviceability limit states where some consequences of actions exceeding the specified service requirements will remain when the actions are removed

reversible serviceability limit states

serviceability limit states where no consequences of actions exceeding the specified service requirements will remain when the actions are removed

serviceability criterion

design criterion for a serviceability limit state

1.5.2.15

resistance

capacity of a member or component, or a cross-section of a member or component of a structure, to withstand actions without mechanical failure e.g. bending resistance, buckling resistance, tension resistance

1.5.2.16

strength

mechanical property of a material indicating its ability to resist actions, usually given in units of stress

1.5.2.17

reliability

ability of a structure or a structural member to fulfill the specified requirements, including the design working life, for which it has been designed. Reliability is usually expressed in probabilistic terms

Note: Reliability covers safety, serviceability and durability of a structure.

1.5.2.18

reliability differentiation

measures intended for the socio-economic optimisation of the resources to be used to build construction works, taking into account all the expected consequences of failures and the cost of the construction works.

1.5.2.19

basic variable

part of a specified set of variables representing physical quantities which characterize actions and environmental influences, geometrical quantities, and material properties including soil properties

1.5.2.20

maintenance

set of activities performed during the working life of the structure in order to enable it to fulfill the requirements for reliability

Note: Activities to restore the structure after an accidental or seismic event are normally outside the scope of maintenance.

1.5.2.21

repair

activities performed to preserve or to restore the function of a structure that fall outside the definition of maintenance

1.5.2.22**nominal value**

value fixed on non-statistical bases, for instance on acquired experience or on physical conditions

1.5.3 Terms relating to actions**1.5.3.1****action (F)**

- a) Set of forces (loads) applied to the structure (direct action);
- b) Set of imposed deformations or accelerations caused for example, by temperature changes, moisture variation, uneven settlement or earthquakes (indirect action).

1.5.3.2**effect of action (E)**

effect of actions (or action effect) on structural members, (e.g. internal force, moment, stress, strain) or on the whole structure (e.g. deflection, rotation)

1.5.3.3**permanent action (G)**

action that is likely to act throughout a given reference period and for which the variation in magnitude with time is negligible, or for which the variation is always in the same direction (monotonic) until the action attains a certain limit value

1.5.3.4**variable action (Q)**

action for which the variation in magnitude with time is neither negligible nor monotonic

1.5.3.5**accidental action (A)**

action, usually of short duration but of significant magnitude, that is unlikely to occur on a given structure during the design working life

Note 1: An accidental action can be expected in many cases to cause severe consequences unless appropriate measures are taken.

Note 2: Impact, snow, wind and seismic actions may be variable or accidental actions, depending on the available information on statistical distributions.

1.5.3.6**seismic action (A_E)**

action that arises due to earthquake ground motions

1.5.3.7**geotechnical action**

action transmitted to the structure by the ground, fill or groundwater

1.5.3.8**fixed action**

action that has a fixed distribution and position over the structure or structural member such that the magnitude and direction of the action are determined unambiguously for the whole

structure or structural member if this magnitude and direction are determined at one point on the structure or structural member

1.5.3.9

free action

action that may have various spatial distributions over the structure

1.5.3.10

single action

action that can be assumed to be statistically independent in time and space of any other action acting on the structure

1.5.3.11

static action

action that does not cause significant acceleration of the structure or structural members

1.5.3.12

dynamic action

action that causes significant acceleration of the structure or structural members

1.5.3.13

quasi-static action

dynamic action represented by an equivalent static action in a static model

1.5.3.14

characteristic value of an action (F_k)

principal representative value of an action

Note: In so far as a characteristic value can be fixed on statistical bases, it is chosen so as to correspond to a prescribed probability of not being exceeded on the unfavourable side during a "reference period" taking into account the design working life of the structure and the duration of the design situation.

1.5.3.15

reference period

chosen period of time that is used as a basis for assessing statistically variable actions, and possibly for accidental actions

1.5.3.16

combination value of a variable action ($\psi_0 Q_k$)

value chosen - in so far as it can be fixed on statistical bases - so that the probability that the effects caused by the combination will be exceeded is approximately the same as by the characteristic value of an individual action. It may be expressed as a determined part of the characteristic value by using a factor $\psi_0 \leq 1$

1.5.3.17

frequent value of a variable action ($\psi_1 Q_k$)

value determined - in so far as it can be fixed on statistical bases - so that either the total time, within the reference period, during which it is exceeded is only a small given part of

the reference period, or the frequency of it being exceeded is limited to a given value. It may be expressed as a determined part of the characteristic value by using a factor $\psi_1 \leq 1$

1.5.3.18

quasi-permanent value of a variable action ($\psi_2 Q_k$)

value determined so that the total period of time for which it will be exceeded is a large fraction of the reference period. It may be expressed as a determined part of the characteristic value by using a factor $\psi_2 \leq 1$

1.5.3.19

accompanying value of a variable action (ψQ_k)

value of a variable action that accompanies the leading action in a combination

Note: The accompanying value of a variable action may be the combination value, the frequent value or the quasi-permanent value.

1.5.3.20

representative value of an action (F_{rep})

value used for the verification of a limit state. A representative value may be the characteristic value (F_k) or an accompanying value (ψF_k)

1.5.3.21

design value of an action (F_d)

value obtained by multiplying the representative value by the partial factor γ_F

Note: The product of the representative value multiplied by the partial factor $\gamma_F = \gamma_{sd} \times \gamma_f$ may also be designated as the design value of the action (See 6.3.2).

1.5.3.22

combination of actions

set of design values used for the verification of the structural reliability for a limit state under the simultaneous influence of different actions

1.5.4 Terms relating to material and product properties

1.5.4.1

characteristic value (X_k or R_k)

value of a material or product property having a prescribed probability of not being attained in a hypothetical unlimited test series. This value generally corresponds to a specified fractile of the assumed statistical distribution of the particular property of the material or product. A nominal value is used as the characteristic value in some circumstances

1.5.4.2

design value of a material or product property (X_d or R_d)

value obtained by dividing the characteristic value by a partial factor γ_m or γ_M , or, in special circumstances, by direct determination

1.5.4.3**nominal value of a material or product property (X_{nom} or R_{nom})**

value normally used as a characteristic value and established from an appropriate document such as a Ethiopian Standard.

1.5.5 Terms relating to geometrical data**1.5.5.1****characteristic value of a geometrical property (a_k)**

value usually corresponding to the dimensions specified in the design. Where relevant, values of geometrical quantities may correspond to some prescribed fractiles of the statistical distribution

1.5.5.2**design value of a geometrical property (a_d)**

generally a nominal value. Where relevant, values of geometrical quantities may correspond to some prescribed fractile of the statistical distribution

Note: The design value of a geometrical property is generally equal to the characteristic value. However, it may be treated differently in cases where the limit state under consideration is very sensitive to the value of the geometrical property, for example when considering the effect of geometrical imperfections on buckling. In such cases, the design value will normally be established as a value specified directly, for example in an appropriate Ethiopian Standard. Alternatively, it can be established from a statistical basis, with a value corresponding to a more appropriate fractile (e.g. a rarer value) than applies to the characteristic value.

1.5.6 Terms relating to structural analysis

Note: The definitions contained in the clause may not necessarily relate to terms used in ES EN 1990:2015, but are included here to ensure a harmonisation of terms relating to structural analysis for ES EN 1991:2015 to ES EN 1998:2015.

1.5.6.1**structural analysis**

procedure or algorithm for determination of action effects in every point of a structure

Note: A structural analysis may have to be performed at three levels using different models: global analysis, member analysis, local analysis.

1.5.6.2**global analysis**

determination, in a structure, of a consistent set of either internal forces and moments, or stresses, that are in equilibrium with a particular defined set of actions on the structure, and depend on geometrical, structural and material properties

1.5.6.3**first order linear-elastic analysis without redistribution**

elastic structural analysis based on linear stress/strain or moment/curvature laws and performed on the initial geometry

1.5.6.4**first order linear-elastic analysis with redistribution**

linear elastic analysis in which the internal moments and forces are modified for structural design, consistently with the given external actions and without more explicit calculation of the rotation capacity

1.5.6.5**second order linear-elastic analysis**

elastic structural analysis, using linear stress/strain laws, applied to the geometry of the deformed structure

1.5.6.6**first order non-linear analysis**

structural analysis, performed on the initial geometry, that takes account of the non-linear deformation properties of materials

Note: First order non-linear analysis is either elastic with appropriate assumptions, or elastic-perfectly plastic (see 1.5.6.8 and 1.5.6.9), or elasto-plastic (see 1.5.6.10) or rigid-plastic (see 1.5.6.11).

1.5.6.7**second order non-linear analysis**

structural analysis, performed on the geometry of the deformed structure, that takes account of the non-linear deformation properties of materials

Note: Second order non-linear analysis is either elastic-perfectly plastic or elasto-plastic.

1.5.6.8**first order elastic-perfectly plastic analysis**

structural analysis based on moment/curvature relationships consisting of a linear elastic part followed by a plastic part without hardening, performed on the initial geometry of the structure

1.5.6.9**second order elastic-perfectly plastic analysis**

structural analysis based on moment/curvature relationships consisting of a linear elastic part followed by a plastic part without hardening, performed on the geometry of the displaced (or deformed) structure

1.5.6.10**elasto-plastic analysis (first or second order)**

structural analysis that uses stress-strain or moment/curvature relationships consisting of a linear elastic part followed by a plastic part with or without hardening

Note: In general, it is performed on the initial structural geometry, but it may also be applied to the geometry of the displaced (or deformed) structure.

1.5.6.11**rigid plastic analysis**

analysis, performed on the initial geometry of the structure, that uses limit analysis theorems for direct assessment of the ultimate loading

Note: The moment/curvature law is assumed without elastic deformation and without hardening.

1.6 Symbols

For the purposes of this Ethiopian Standard, the following symbols apply.

Note: The notation used is based on ES ISO 3898:1987

Latin upper case letters

A	Accidental action
A_d	Design value of an accidental action
A_{Ed}	Design value of seismic action $A_{Ed} = \gamma_I A_{Ek}$
A_{Ek}	Characteristic value of seismic action
C_d	Nominal value, or a function of certain design properties of materials
E	Effect of actions
E_d	Design value of effect of actions
$E_{d,dst}$	Design value of effect of destabilising actions
$E_{d,stab}$	Design value of effect of stabilising actions
F	Action
F_d	Design value of an action
F_k	Characteristic value of an action
F_{rep}	Representative value of an action
G	Permanent action
G_d	Design value of a permanent action
$G_{d,inf}$	Lower design value of a permanent action
$G_{d,sup}$	Upper design value of a permanent action
G_k	Characteristic value of a permanent action
$G_{k,j}$	Characteristic value of permanent action j
$G_{kj,sup} / G_{kj,inf}$	Upper/lower characteristic value of permanent action j
P	Relevant representative value of a prestressing action (see ES EN 1992:2015 to ES EN 1996:2015 and ES EN 1998:2015)
P_d	Design value of a prestressing action
P_k	Characteristic value of a prestressing action
P_m	Mean value of a prestressing action
Q	Variable action
Q_d	Design value of a variable action
Q_k	Characteristic value of a single variable action
$Q_{k,1}$	Characteristic value of the leading variable action 1
$Q_{k,i}$	Characteristic value of the accompanying variable action i
R	Resistance
R_d	Design value of the resistance

R_k	Characteristic value of the resistance
X	Material property
X_d	Design value of a material property
X_k	Characteristic value of a material property

Latin lower case letters

a_d	Design values of geometrical data
a_k	Characteristic values of geometrical data
a_{nom}	Nominal value of geometrical data
u	Horizontal displacement of a structure or structural member
w	Vertical deflection of a structural member

Greek upper case letters

Δa	Change made to nominal geometrical data for particular design purposes, e.g. assessment of effects of imperfections
------------	---

Greek lower case letters

γ	Partial factor (safety or serviceability)
γ_f	Partial factor for actions, which takes account of the possibility of unfavourable deviations of the action values from the representative values
γ_F	Partial factor for actions, also accounting for model uncertainties and dimensional variations
γ_g	Partial factor for permanent actions, which takes account of the possibility of unfavourable deviations of the action values from the representative values
γ_G	Partial factor for permanent actions, also accounting for model uncertainties and dimensional variations
$\gamma_{G,j}$	Partial factor for permanent action j
$\gamma_{Gj,sup} / \gamma_{Gj,inf}$	Partial factor for permanent action j in calculating upper/lower design values
γ_I	Importance factor (see ES EN 1998:2015)
γ_m	Partial factor for a material property
γ_M	Partial factor for a material property, also accounting for model uncertainties and dimensional variations
γ_P	Partial factor for prestressing actions (see ES EN 1992:2015 to ES EN 1996:2015 and ES EN 1998:2015)
γ_q	Partial factor for variable actions, which takes account of the possibility of unfavourable deviations of the action values from the representative values
γ_Q	Partial factor for variable actions, also accounting for model uncertainties and dimensional variations
$\gamma_{Q,i}$	Partial factor for variable action i

γ_{Rd}	Partial factor associated with the uncertainty of the resistance model
γ_{Sd}	Partial factor associated with the uncertainty of the action and/or action effect model
η	Conversion factor
ξ	Reduction factor
ψ_0	Factor for combination value of a variable action
ψ_1	Factor for frequent value of a variable action
ψ_2	Factor for quasi-permanent value of a variable action

SECTION 2. REQUIREMENTS

2.1 Basic requirements

(1)P A structure shall be designed and executed in such a way that it will, during its intended life, with appropriate degrees of reliability and in an economical way

- sustain all actions and influences likely to occur during execution and use, and
- remain fit for the use for which it is required.

(2)P A structure shall be designed to have adequate:

- structural resistance,
- serviceability, and
- durability.

(3)P In the case of fire, the structural resistance shall be adequate for the required period of time.

Note: See also ES EN 1991-1-2:2015

(4)P A structure shall be designed and executed in such a way that it will not be damaged by events such as :

- explosion,
- impact, and
- the consequences of human errors,

to an extent disproportionate to the original cause.

Note 1: The events to be taken into account are those agreed for an individual project with the client and the relevant authority.

Note 2: Further information is given in ES EN 1991-1-7:2015.

(5)P Potential damage shall be avoided or limited by appropriate choice of one or more of the following :

- avoiding, eliminating or reducing the hazards to which the structure can be subjected;
- selecting a structural form which has low sensitivity to the hazards considered;
- selecting a structural form and design that can survive adequately the accidental removal of an individual member or a limited part of the structure, or the occurrence of acceptable localised damage;
- avoiding as far as possible structural systems that can collapse without warning;
- tying the structural members together.

(6) The basic requirements should be met:

- by the choice of suitable materials,
- by appropriate design and detailing, and
- by specifying control procedures for design, production, execution, and use relevant to the particular project.

(7) The provisions of Section 2 should be interpreted on the basis that due skill and care appropriate to the circumstances is exercised in the design, based on such knowledge and good practice as is generally available at the time that the design of the structure is carried out.

2.2 Reliability management

(1)P The reliability required for structures within the scope of ES EN 1990:2015 shall be achieved:

a) by design in accordance with ES EN 1990:2015 to ES EN 1998:2015 and

b) by

- appropriate execution and
- quality management measures.

Note: See 2.2(5) and Annex B

(2) Different levels of reliability may be adopted inter alia:

- for structural resistance;
- for serviceability.

(3) The choice of the levels of reliability for a particular structure should take account of the relevant factors, including:

- the possible cause and /or mode of attaining a limit state;
- the possible consequences of failure in terms of risk to life, injury, potential economical losses;
- public aversion to failure;
- the expense and procedures necessary to reduce the risk of failure.

(4) The levels of reliability that apply to a particular structure may be specified in one or both of the following ways :

- by the classification of the structure as a whole;
- by the classification of its components.

Note: See also Annex B

(5) The levels of reliability relating to structural resistance and serviceability can be achieved by suitable combinations of:

a) preventative and protective measures (e.g. implementation of safety barriers, active and passive protective measures against fire, protection against risks of corrosion such as painting or cathodic protection);

b) measures relating to design calculations:

- representative values of actions;
- the choice of partial factors;

- c) measures relating to quality management;
- d) measures aimed to reduce errors in design and execution of the structure, and gross human errors;
- e) other measures relating to the following other design matters:
- the basic requirements;
 - the degree of robustness (structural integrity);
 - durability, including the choice of the design working life;
 - the extent and quality of preliminary investigations of soils and possible environmental influences;
 - the accuracy of the mechanical models used ;
 - the detailing;
- f) efficient execution, e.g. in accordance with execution standards referred to in ES EN 1991:2015 to ES EN 1998:2015.
- g) adequate inspection and maintenance according to procedures specified in the project documentation.

(6) The measures to prevent potential causes of failure and/or reduce their consequences may, in appropriate circumstances, be interchanged to a limited extent provided that the required reliability levels are maintained.

2.3 Design working life

(1) The design working life should be specified.

Note: Indicative categories are given in Table 2.1. The values given in Table 2.1 may also be used for determining time-dependent performance (e.g. fatigue-related calculations). See also Annex A.

Table 2.1 - Indicative design working life

Design working life category	Indicative design working life (years)	Examples
1	10	Temporary structures ⁽¹⁾
2	10 to 25	Replaceable structural parts, e.g. gantry girders, bearings
3	15 to 30	Agricultural and similar structures
4	50	Building structures and other common structures
5	100	Monumental building structures, bridges, and other civil engineering structures
(1) Structures or parts of structures that can be dismantled with a view to being re-used should not be considered as temporary.		

2.4 Durability

(1)P The structure shall be designed such that deterioration over its design working life does not impair the performance of the structure below that intended, having due regard to its environment and the anticipated level of maintenance.

(2) In order to achieve an adequately durable structure, the following should be taken into account :

- the intended or foreseeable use of the structure ;
- the required design criteria ;
- the expected environmental conditions ;
- the composition, properties and performance of the materials and products ;
- the properties of the soil ;
- the choice of the structural system ;
- the shape of members and the structural detailing ;
- the quality of workmanship, and the level of control ;
- the particular protective measures ;
- the intended maintenance during the design working life.

Note: The relevant ES EN 1992:2015 to ES EN 1998:2015 specify appropriate measures to reduce deterioration.

(3)P The environmental conditions shall be identified at the design stage so that their significance can be assessed in relation to durability and adequate provisions can be made for protection of the materials used in the structure.

(4)The degree of any deterioration may be estimated on the basis of calculations, experimental investigation, experience from earlier constructions, or a combination of these considerations.

2.5 Quality management

(1) In order to provide a structure that corresponds to the requirements and to the assumptions made in the design, appropriate quality management measures should be in place. These measures comprise:

- definition of the reliability requirements,
- organisational measures and
- controls at the stages of design, execution, use and maintenance.

Note: ES ISO 9001:2000 is an acceptable basis for quality management measures, where relevant.

SECTION 3. PRINCIPLES OF LIMIT STATES DESIGN

3.1 General

(1)P A distinction shall be made between ultimate limit states and serviceability limit states.

Note: In some cases, additional verifications may be needed, for example to ensure traffic safety.

(2) Verification of one of the two categories of limit states may be omitted provided that sufficient information is available to prove that it is satisfied by the other.

(3)P Limit states shall be related to design situations, see 3.2.

(4) Design situations should be classified as persistent, transient or accidental, see 3.2.

(5) Verification of limit states that are concerned with time dependent effects (e.g. fatigue) should be related to the design working life of the construction.

Note: Most time dependent effects are cumulative.

3.2 Design situations

(1)P The relevant design situations shall be selected taking into account the circumstances under which the structure is required to fulfill its function.

(2)P Design situations shall be classified as follows:

- persistent design situations, which refer to the conditions of normal use;
- transient design situations, which refer to temporary conditions applicable to the structure, e.g. during execution or repair ;
- accidental design situations, which refer to exceptional conditions applicable to the structure or to its exposure, e.g. to fire, explosion, impact or the consequences of localized failure;
- seismic design situations, which refer to conditions applicable to the structure when subjected to seismic events.

Note: Information on specific design situations within each of these classes is given in ES EN 1991:2015 to ES EN 1998:2015.

(3)P The selected design situations shall be sufficiently severe and varied so as to encompass all conditions that can reasonably be foreseen to occur during the execution and use of the structure.

3.3 Ultimate limit states

(1)P The limit states that concern:

- the safety of people, and/or
 - the safety of the structure
- shall be classified as ultimate limit states.

(2) In some circumstances, the limit states that concern the protection of the contents should be classified as ultimate limit states.

Note: The circumstances are those agreed for a particular project with the client and the relevant authority.

(3) States prior to structural collapse, which, for simplicity, are considered in place of the collapse itself, may be treated as ultimate limit states.

(4) The following ultimate limit states shall be verified where they are relevant:

- loss of equilibrium of the structure or any part of it, considered as a rigid body;
- failure by excessive deformation, transformation of the structure or any part of it into a mechanism, rupture, loss of stability of the structure or any part of it, including supports and foundations;
- failure caused by fatigue or other time-dependent effects.

Note: Different sets of partial factors are associated with the various ultimate limit states, see 6.4.1. Failure due to excessive deformation is structural failure due to mechanical instability.

3.4 Serviceability limit states

(1) The limit states that concern:

- the functioning of the structure or structural members under normal use ;
 - the comfort of people ;
 - the appearance of the construction works,
- shall be classified as serviceability limit states.

Note 1: In the context of serviceability, the term “appearance” is concerned with such criteria as high deflection and extensive cracking, rather than aesthetics.

Note 2: Usually the serviceability requirements are agreed for each individual project.

(2) A distinction shall be made between reversible and irreversible serviceability limit states.

(3) The verification of serviceability limit states should be based on criteria concerning the following aspects:

- a) deformations that affect
- the appearance,
 - the comfort of users, or
 - the functioning of the structure (including the functioning of machines or services),

or that cause damage to finishes or non-structural members;

- b) vibrations

- that cause discomfort to people, or
- that limit the functional effectiveness of the structure;

- c) damage that is likely to adversely affect

- the appearance,

- the durability, or
- the functioning of the structure.

Note: Additional provisions related to serviceability criteria are given in the relevant ES EN 1992:2015 to ES EN 1998:2015.

3.5 Limit state design

(1)P Design for limit states shall be based on the use of structural and load models for relevant limit states.

(2)P It shall be verified that no limit state is exceeded when relevant design values for

- actions,
 - material properties, or
 - product properties, and
 - geometrical data
- are used in these models.

(3)P The verifications shall be carried out for all relevant design situations and load cases.

(4) The requirements of 3.5(1)P should be achieved by the partial factor method, described in section 6.

(5) As an alternative, a design directly based on probabilistic methods may be used.

Note 1: The relevant authority can give specific conditions for use.

Note 2: For a basis of probabilistic methods, see Annex C.

(6)P The selected design situations shall be considered and critical load cases identified.

(7) For a particular verification load cases should be selected, identifying compatible load arrangements, sets of deformations and imperfections that should be considered simultaneously with fixed variable actions and permanent actions.

(8)P Possible deviations from the assumed directions or positions of actions shall be taken into account.

(9) Structural and load models can be either physical models or mathematical models.

SECTION 4. BASIC VARIABLES

4.1 Actions and environmental influences

4.1.1 Classification of actions

(1)P Actions shall be classified by their variation in time as follows:

- permanent actions (G), e.g. self-weight of structures, fixed equipment and road surfacing, and indirect actions caused by shrinkage and uneven settlements ;
- variable actions (Q), e.g. imposed loads on building floors, beams and roofs, wind actions or snow loads ;
- accidental actions (A), e.g. explosions, or impact from vehicles.

Note: Indirect actions caused by imposed deformations can be either permanent or variable.

(2) Certain actions, such as seismic actions and snow loads, may be considered as either accidental and/or variable actions, depending on the site location, see ES EN 1991:2015 and ES EN 1998:2015.

(3) Actions caused by water may be considered as permanent and/or variable actions depending on the variation of their magnitude with time.

(4)P Actions shall also be classified

- by their origin, as direct or indirect,
- by their spatial variation, as fixed or free, or
- by their nature and/or the structural response, as static or dynamic.

(5) An action should be described by a model, its magnitude being represented in the most common cases by one scalar which may have several representative values.

Note: For some actions and some verifications, a more complex representation of the magnitudes of some actions may be necessary.

4.1.2 Characteristic values of actions

(1)P The characteristic value F_k of an action is its main representative value and shall be specified :

- as a mean value, an upper or lower value, or a nominal value (which does not refer to a known statistical distribution) (see ES EN 1991:2015) ;
- in the project documentation, provided that consistency is achieved with methods given in ES EN 1991:2015.

(2)P The characteristic value of a permanent action shall be assessed as follows:

- if the variability of G can be considered as small, one single value G_k may be used;
- if the variability of G cannot be considered as small, two values shall be used: an upper value $G_{k,\text{sup}}$ and a lower value $G_{k,\text{inf}}$.

(3) The variability of G may be neglected if G does not vary significantly during the design working life of the structure and its coefficient of variation is small. \bar{G}_k should then be taken equal to the mean value.

Note: This coefficient of variation can be in the range of 0.05 to 0.10 depending on the type of structure.

(4) In cases when the structure is very sensitive to variations in G (e.g. some types of prestressed concrete structures), two values should be used even if the coefficient of variation is small. Then $G_{k,inf}$ is the 5% fractile and $G_{k,sup}$ is the 95% fractile of the statistical distribution for G , which may be assumed to be Gaussian.

(5) The self-weight of the structure may be represented by a single characteristic value and be calculated on the basis of the nominal dimensions and mean unit masses, see ES EN 1991-1-1:2015.

Note: For the settlement of foundations, see ES EN 1997:2015.

(6) Prestressing (P) should be classified as a permanent action caused by either controlled forces and/or controlled deformations imposed on a structure. These types of prestress should be distinguished from each other as relevant (e.g. prestress by tendons, prestress by imposed deformation at supports).

Note: The characteristic values of prestress, at a given time t , may be an upper value $P_{k,sup}(t)$ and a lower value $P_{k,inf}(t)$. For ultimate limit states, a mean value $P_m(t)$ can be used. Detailed information is given in ES EN 1992:2015 to ES EN 1996:2015.

(7)P For variable actions, the characteristic value (Q_k) shall correspond to either:

- an upper value with an intended probability of not being exceeded or a lower value with an intended probability of being achieved, during some specific reference period;
- a nominal value, which may be specified in cases where a statistical distribution is not known.

Note 1: Values are given in the various Parts of ES EN 1991:2015.

Note 2: The characteristic value of climatic actions is based upon the probability of 0.02 of its time varying part being exceeded for a reference period of one year. This is equivalent to a mean return period of 50 years for the time-varying part. However in some cases the character of the action and/or the selected design situation makes another fractile and/or return period more appropriate.

(8) For accidental actions the design value A_d should be specified for individual projects.

Note: See also ES EN 1991-1-7:2015.

(9) For seismic actions the design value A_{Ed} should be assessed from the characteristic value A_{Ek} or specified for individual projects.

Note: See also ES EN 1998:2015.

(10) For multi-component actions the characteristic action should be represented by groups of values each to be considered separately in design calculations.

4.1.3 Other representative values of variable actions

(1)P Other representative values of a variable action shall be as follows:

- (a) the combination value, represented as a product $\psi_0 Q_k$ used for the verification of ultimate limit states and irreversible serviceability limit states (see section 6 and Annex C) ;
- (b) the frequent value, represented as a product $\psi_1 Q_k$ used for the verification of ultimate limit states involving accidental actions and for verifications of reversible serviceability limit states;

Note 1: For buildings, for example, the frequent value is chosen so that the time it is exceeded is 0.01 of the reference period; for road traffic loads on bridges, the frequent value is assessed on the basis of a return period of one week.

Note 2: The infrequent value, represented as a product $\psi_{1,inf} Q_k$, is used for the verification of certain serviceability limit states specifically for concrete bridge decks, or concrete parts of bridge decks. The infrequent value, defined only for road traffic loads (see ES EN 1991-2:2015) thermal actions (see ES EN 1991-1-5:2015) and wind actions (see ES EN 1991-1-4:2015), is based on a return period of one year.

- (c) the quasi-permanent value, represented as a product $\psi_2 Q_k$, used for the verification of ultimate limit states involving accidental actions and for the verification of reversible serviceability limit states. Quasi-permanent values are also used for the calculation of long-term effects.

Note: For loads on building floors, the quasi-permanent value is usually chosen so that the proportion of the time it is exceeded is 0.50 of the reference period. The quasi-permanent value can alternatively be determined as the value averaged over a chosen period of time. In the case of wind actions or road traffic loads, the quasi-permanent value is generally taken as zero.

4.1.4 Representation of fatigue actions

(1) The models for fatigue actions should be those that have been established in the relevant parts of ES EN 1991:2015 from evaluation of structural responses to fluctuations of loads performed for common structures (e.g. for simple span and multi-span bridges, tall slender structures for wind).

(2) For structures outside the field of application of models established in the relevant Parts of ES EN 1991:2015, fatigue actions should be defined from the evaluation of measurements or equivalent studies of the expected action spectra.

Note: For the consideration of material specific effects (for example, the consideration of mean stress influence or non-linear effects), see ES EN 1992:2015 to ES EN 1998:2015.

4.1.5 Representation of dynamic actions

(1) The characteristic and fatigue load models in ES EN 1991:2015 include the effects of accelerations caused by the actions either implicitly in the characteristic loads or explicitly by applying dynamic enhancement factors to characteristic static loads.

Note: Limits of use of these models are described in the various Parts of ES EN 1991:2015.

(2) When dynamic actions cause significant acceleration of the structure, dynamic analysis of the system should be used. See 5.1.3 (6).

4.1.6 Geotechnical actions

(1)P Geotechnical actions shall be assessed in accordance with ES EN 1997-1:2015.

4.1.7 Environmental influences

(1)P The environmental influences that could affect the durability of the structure shall be considered in the choice of structural materials, their specification, the structural concept and detailed design.

Note: The ES EN 1992:2015 to ES EN 1998:2015 give the relevant measures.

(2) The effects of environmental influences should be taken into account, and where possible, be described quantitatively.

4.2 Material and product properties

(1) Properties of materials (including soil and rock) or products should be represented by characteristic values (see 1.5.4.1).

(2) When a limit state verification is sensitive to the variability of a material property, upper and lower characteristic values of the material property should be taken into account.

(3) Unless otherwise stated in ES EN 1991:2015 to ES EN 1998:2015 :

- where a low value of material or product property is unfavourable, the characteristic value should be defined as the 5% fractile value;
- where a high value of material or product property is unfavourable, the characteristic value should be defined as the 95% fractile value.

(4)P Material property values shall be determined from standardised tests performed under specified conditions. A conversion factor shall be applied where it is necessary to convert the test results into values which can be assumed to represent the behaviour of the material or product in the structure or the ground.

Note: See annex D and ES EN 1992:2015 to ES EN 1998:2015

(5) Where insufficient statistical data are available to establish the characteristic values of a material or product property, nominal values may be taken as the characteristic values, or design values of the property may be established directly. Where upper or lower design values of a material or product property are established directly (e.g. friction factors, damping ratios), they should be selected so that more adverse values would affect the probability of occurrence of the limit state under consideration to an extent similar to other design values.

(6) Where an upper estimate of strength is required (e.g. for capacity design measures and for the tensile strength of concrete for the calculation of the effects of indirect actions) a characteristic upper value of the strength should be taken into account.

(7) The reductions of the material strength or product resistance to be considered resulting from the effects of repeated actions are given in ES EN 1992:2015 to ES EN 1998:2015 and can lead to a reduction of the resistance over time due to fatigue.

(8) The structural stiffness parameters (e.g. moduli of elasticity, creep coefficients) and thermal expansion coefficients should be represented by a mean value. Different values should be used to take into account the duration of the load.

Note: In some cases, a lower or higher value than the mean for the modulus of elasticity may have to be taken into account (e.g. in case of instability).

(9) Values of material or product properties are given in ES EN 1992:2015 to ES EN 1998:2015. If values are taken from product standards without guidance on interpretation being given in ES EN 1992:2015 to ES EN 1998:2015, the most adverse values should be used.

(10)P Where a partial factor for materials or products is needed, a conservative value shall be used, unless suitable statistical information exists to assess the reliability of the value chosen.

Note: Suitable account may be taken where appropriate of the unfamiliarity of the application or materials/products used.

4.3 Geometrical data

(1)P Geometrical data shall be represented by their characteristic values, or (e.g. the case of imperfections) directly by their design values.

(2) The dimensions specified in the design may be taken as characteristic values.

(3) Where their statistical distribution is sufficiently known, values of geometrical quantities that correspond to a prescribed fractile of the statistical distribution may be used.

(4) Imperfections that should be taken into account in the design of structural members are given in ES EN 1992:2015 to ES EN 1998:2015.

(5)P Tolerances for connected parts that are made from different materials shall be mutually compatible.

SECTION 5. STRUCTURAL ANALYSIS AND DESIGN ASSISTED BY TESTING

5.1 Structural analysis

5.1.1 Structural modelling

(1)P Calculations shall be carried out using appropriate structural models involving relevant variables.

(2)The structural models selected should be those appropriate for predicting structural behaviour with an acceptable level of accuracy. The structural models should also be appropriate to the limit states considered.

(3)P Structural models shall be based on established engineering theory and practice. If necessary, they shall be verified experimentally.

5.1.2 Static actions

(1)P The modelling for static actions shall be based on an appropriate choice of the force-deformation relationships of the members and their connections and between members and the ground.

(2)P Boundary conditions applied to the model shall represent those intended in the structure.

(3)P Effects of displacements and deformations shall be taken into account in the context of ultimate limit state verifications if they result in a significant increase of the effect of actions.

Note: Particular methods for dealing with effects of deformations are given in ES EN 1991:2015 to ES EN 1998:2015.

(4)P Indirect actions shall be introduced in the analysis as follows:

- in linear elastic analysis, directly or as equivalent forces (using appropriate modular ratios where relevant) ;
- in non-linear analysis, directly as imposed deformations.

5.1.3 Dynamic actions

(1)P The structural model to be used for determining the action effects shall be established taking account of all relevant structural members, their masses, strengths, stiffnesses and damping characteristics, and all relevant nonstructural members with their properties.

(2)P The boundary conditions applied to the model shall be representative of those intended in the structure.

(3) When it is appropriate to consider dynamic actions as quasi-static, the dynamic parts may be considered either by including them in the static values or by applying equivalent dynamic amplification factors to the static actions.

Note: For some equivalent dynamic amplification factors, the natural frequencies are determined.

(4) In the case of ground-structure interaction, the contribution of the soil may be modeled by appropriate equivalent springs and dash-pots.

(5) Where relevant (e.g. for wind induced vibrations or seismic actions) the actions may be defined by a modal analysis based on linear material and geometric behaviour. For structures that have regular geometry, stiffness and mass distribution, provided that only the fundamental mode is relevant, an explicit modal analysis may be substituted by an analysis with equivalent static actions.

(6) The dynamic actions may be also expressed, as appropriate, in terms of time histories or in the frequency domain, and the structural response determined by appropriate methods.

(7) Where dynamic actions cause vibrations of a magnitude or frequencies that could exceed serviceability requirements, a serviceability limit state verification should be carried out.

Note: Guidance for assessing these limits is given in Annex A and ES EN 1992:2015 to ES EN 1998:2015.

5.1.4 Fire design

(1)P The structural fire design analysis shall be based on design fire scenarios (see ES EN 1991-1-2:2015), and shall consider models for the temperature evolution within the structure as well as models for the mechanical behaviour of the structure at elevated temperature.

(2) The required performance of the structure exposed to fire should be verified by either global analysis, analysis of sub-assemblies or member analysis, as well as the use of tabular data or test results.

(3) The behaviour of the structure exposed to fire should be assessed by taking into account either:

- nominal fire exposure, or
 - modelled fire exposure,
- as well as the accompanying actions.

Note: See also ES EN 1991-1-2:2015.

(4) The structural behaviour at elevated temperatures should be assessed in accordance with ES EN 1992:2015 to ES EN 1996:2015, which give thermal and structural models for analysis.

(5) Where relevant to the specific material and the method of assessment:

- thermal models may be based on the assumption of a uniform or a non-uniform temperature within cross-sections and along members;
- structural models may be confined to an analysis of individual members or may account for the interaction between members in fire exposure.

(6) The models of mechanical behaviour of structural members at elevated temperatures should be non-linear.

Note: See also ES EN 1991:2015 to ES EN 1998:2015.

5.2 Design assisted by testing

(1) Design may be based on a combination of tests and calculations.

Note: Testing may be carried out, for example, in the following circumstances :

- if adequate calculation models are not available;
- if a large number of similar components are to be used;
- to confirm by control checks assumptions made in the design.

See Annex D.

(2)P Design assisted by test results shall achieve the level of reliability required for the relevant design situation. The statistical uncertainty due to a limited number of test results shall be taken into account.

(3) Partial factors (including those for model uncertainties) comparable to those used in ES EN 1991:2015 to ES EN 1998:2015 should be used.

SECTION 6. VERIFICATION BY THE PARTIAL FACTOR METHOD

6.1 General

(1)P When using the partial factor method, it shall be verified that, in all relevant design situations, no relevant limit state is exceeded when design values for actions or effects of actions and resistances are used in the design models.

(2) For the selected design situations and the relevant limit states the individual actions for the critical load cases should be combined as detailed in this section. However actions that cannot occur simultaneously, for example due to physical reasons, should not be considered together in combination.

(3) Design values should be obtained by using:

- the characteristic, or
- other representative values,

in combination with partial and other factors as defined in this section and ES EN 1991:2015 to ES EN 1998:2015.

(4) It can be appropriate to determine design values directly where conservative values should be chosen.

(5)P Design values directly determined on statistical bases shall correspond to at least the same degree of reliability for the various limit states as implied by the partial factors given in this standard.

6.2 Limitations

(1) The use of the Application Rules given in ES EN 1990:2015 is limited to ultimate and serviceability limit state verifications of structures subject to static loading, including cases where the dynamic effects are assessed using equivalent quasi-static loads and dynamic amplification factors, including wind or traffic loads. For non-linear analysis and fatigue the specific rules given in various Parts of ES EN 1991:2015 to ES EN 1998:2015 should be applied.

6.3 Design values

6.3.1 Design values of actions

(1) The design value F_d of an action F can be expressed in general terms as:

$$F_d = \gamma_f F_{rep} \quad (6.1a)$$

with :

$$F_{rep} = \psi F_k \quad (6.1b)$$

where:

F_k is the characteristic value of the action.

F_{rep} is the relevant representative value of the action.

γ_f is a partial factor for the action which takes account of the possibility of unfavourable deviations of the action values from the representative values.

ψ is either 1.00 or ψ_0 , ψ_1 or ψ_2 .

(2) For seismic actions the design value A_{Ed} should be determined taking account of the structural behaviour and other relevant criteria detailed in ES EN 1998:2015.

6.3.2 Design values of the effects of actions

(1) For a specific load case the design values of the effects of actions (E_d) can be expressed in general terms as:

$$E_d = \gamma_{Sd} E \{ \gamma_{f,i} F_{rep,i}; a_d \} \quad i \geq 1 \quad (6.2)$$

where:

a_d is the design values of the geometrical data (see 6.3.4);

γ_{Sd} is a partial factor taking account of uncertainties:

- in modelling the effects of actions ;
- in some cases, in modelling the actions.

Note: In a more general case the effects of actions depend on material properties.

(2) In most cases, the following simplification can be made:

$$E_d = E \{ \gamma_{F,i} F_{rep,i}; a_d \} \quad i \geq 1 \quad (6.2a)$$

with:

$$\gamma_{F,i} = \gamma_{Sd} \times \gamma_{f,i} \quad (6.2b)$$

Note: When relevant, e.g. where geotechnical actions are involved, partial factors $\gamma_{F,i}$ can be applied to the effects of individual actions or only one particular factor γ_F can be globally applied to the effect of the combination of actions with appropriate partial factors.

(3)P Where a distinction has to be made between favourable and unfavourable effects of permanent actions, two different partial factors shall be used ($\gamma_{G,inf}$ and $\gamma_{G,sup}$).

(4) For non-linear analysis (i.e. when the relationship between actions and their effects is not linear), the following simplified rules may be considered in the case of a single predominant action:

- a) When the action effect increases more than the action, the partial factor γ_F should be applied to the representative value of the action.
- b) When the action effect increases less than the action, the partial factor γ_F should be applied to the action effect of the representative value of the action.

Note: Except for rope, cable and membrane structures, most structures or structural elements are in category a).

(5) In those cases where more refined methods are detailed in the relevant ES EN 1991:2015 to ES EN 1998:2015 (e.g. for prestressed structures), they should be used in preference to 6.3.2(4).

6.3.3 Design values of material or product properties

(1) The design value X_d of a material or product property can be expressed in general terms as:

$$X_d = \eta \frac{X_k}{\gamma_m} \quad (6.3)$$

where:

X_k is the characteristic value of the material or product property (see 4.2(3)) ;

η is the mean value of the conversion factor taking into account

- volume and scale effects,
- effects of moisture and temperature, and
- any other relevant parameters ;

γ_m is the partial factor for the material or product property to take account of:

- the possibility of an unfavourable deviation of a material or product property from its characteristic value;
- the random part of the conversion factor η .

(2) Alternatively, in appropriate cases, the conversion factor η may be :

- implicitly taken into account within the characteristic value itself, or
- by using γ_M instead of γ_m (see expression (6.6b)).

Note: The design value can be established by such means as :

- empirical relationships with measured physical properties, or
- with chemical composition, or
- from previous experience, or
- from values given in Ethiopian Standards or other appropriate documents.

6.3.4 Design values of geometrical data

(1) Design values of geometrical data such as dimensions of members that are used to assess action effects and/or resistances may be represented by nominal values:

$$a_d = a_{nom} \quad (6.4)$$

(2)P Where the effects of deviations in geometrical data (e.g. inaccuracy in the load application or location of supports) are significant for the reliability of the structure (e.g. by second order effects) the design values of geometrical data shall be defined by:

$$a_d = a_{nom} \pm \Delta a \quad (6.5)$$

where :

Δa takes account of:

- the possibility of unfavourable deviations from the characteristic or nominal values ;
- the cumulative effect of a simultaneous occurrence of several geometrical deviations.

Note 1: a_d can also represent geometrical imperfections where $a_{nom} = 0$ (i.e., $\Delta a \neq 0$).

Note 2: Where relevant, ES EN 1991:2015 to ES EN 1998:2015 provide further provisions.

(3) Effects of other deviations should be covered by partial factors

- on the action side (γ_F), and/or
- resistance side (γ_M).

Note: Tolerances are defined in the relevant standards on execution referred to in ES EN 1990:2015 to ES EN 1998:2015.

6.3.5 Design resistance

(1) The design resistance R_d can be expressed in the following form:

$$R_d = \frac{1}{\gamma_{Rd}} R \{ X_{d,i}; a_d \} = \frac{1}{\gamma_{Rd}} R \left\{ \eta_i \frac{X_{k,i}}{\gamma_{m,i}}; a_d \right\} i \geq 1 \quad (6.6)$$

where:

γ_{Rd} is a partial factor covering uncertainty in the resistance model, plus geometric deviations if these are not modelled explicitly (see 6.3.4(2));

$X_{d,i}$ is the design value of material property i .

(2) The following simplification of expression (6.6) may be made:

$$R_d = R \left\{ \eta_i \frac{X_{k,i}}{\gamma_{M,i}}; a_d \right\} i \geq 1 \quad (6.6a)$$

where :

$$\gamma_{M,i} = \gamma_{Rd} \times \gamma_{m,i} \quad (6.6b)$$

Note: η_i may be incorporated in $\gamma_{M,i}$ see 6.3.3.(2).

(3) Alternatively to expression (6.6a), the design resistance may be obtained directly from the characteristic value of a material or product resistance, without explicit determination of design values for individual basic variables, using :

$$R_d = \frac{R_k}{\gamma_M} \quad (6.6c)$$

Note: This is applicable to products or members made of a single material (e.g. steel) and is also used in connection with Annex D “Design assisted by testing”.

(4) Alternatively to expressions (6.6a) and (6.6c), for structures or structural members that are analysed by non-linear methods, and comprise more than one material acting in association, or where ground properties are involved in the design resistance, the following expression for design resistance can be used:

$$R_d = \frac{1}{\gamma_{M,1}} R \left\{ \eta_1 X_{k,1}; \eta_i X_{k,i(i>1)} \frac{\gamma_{M,1}}{\gamma_{M,i}}; a_d \right\} \quad (6.6d)$$

Note: In some cases, the design resistance can be expressed by applying directly γ_M partial factors to the individual resistances due to material properties.

6.4 Ultimate limit states

6.4.1 General

(1)P The following ultimate limit states shall be verified as relevant :

- a) EQU : Loss of static equilibrium of the structure or any part of it considered as a rigid body, where:
 - minor variations in the value or the spatial distribution of actions from a single source are significant, and
 - the strengths of construction materials or ground are generally not governing;
- b) STR: Internal failure or excessive deformation of the structure or structural members, including footings, piles, basement walls, etc., where the strength of construction materials of the structure governs;
- c) GEO: Failure or excessive deformation of the ground where the strengths of soil or rock are significant in providing resistance ;
- d) FAT: Fatigue failure of the structure or structural members.

Note: For fatigue design, the combinations of actions are given in ES EN 1992:2015 to ES EN 1998:2015.

(2)P The design values of actions shall be in accordance with Annex A.

6.4.2 Verifications of static equilibrium and resistance

(1)P When considering a limit state of static equilibrium of the structure (EQU), it shall be verified that :

$$E_{d,dst} \leq E_{d,stb} \quad (6.7)$$

where:

$E_{d,dst}$ is the design value of the effect of destabilising actions ;

$E_{d,stb}$ is the design value of the effect of stabilising actions.

(2) Where appropriate the expression for a limit state of static equilibrium may be supplemented by additional terms, including, for example, a coefficient of friction between rigid bodies.

(3)P When considering a limit state of rupture or excessive deformation of a section, member or connection (STR and/or GEO), it shall be verified that :

$$E_d \leq R_d \quad (6.8)$$

where:

E_d is the design value of the effect of actions such as internal force, moment or a vector representing several internal forces or moments;

R_d is the design value of the corresponding resistance.

Note 1: Details for the methods STR and GEO are given in Annex A.

Note 2: Expression (6.8) does not cover all verification formats concerning buckling, i.e. failure that happens where second order effects cannot be limited by the structural response, or by an acceptable structural response. See ES EN 1992:2015 to ES EN 1998:2015.

6.4.3 Combination of actions (fatigue verifications excluded)

6.4.3.1 General

(1)P For each critical load case, the design values of the effects of actions (E_d) shall be determined by combining the values of actions that are considered to occur simultaneously.

(2) Each combination of actions should include:

- a leading variable action, or
- an accidental action.

(3) The combinations of actions should be in accordance with 6.4.3.2 to 6.4.3.4.

(4)P Where the results of a verification are very sensitive to variations of the magnitude of a permanent action from place to place in the structure, the unfavourable and the favourable parts of this action shall be considered as individual actions.

Note: This applies in particular to the verification of static equilibrium and analogous limit states, see 6.4.2(2).

(5) Where several effects of one action (e.g. bending moment and normal force due to selfweight) are not fully correlated, the partial factor applied to any favourable component may be reduced.

Note: For further guidance on this topic see the clauses on vectorial effects in ES EN 1992:2015 to ES EN 1998:2015.

(6) Imposed deformations should be taken into account where relevant.

Note: For further guidance, see 5.1.2.4(P) and ES EN 1992:2015 to ES EN 1998:2015.

6.4.3.2 Combinations of actions for persistent or transient design situations (fundamental combinations)

(1) The general format of effects of actions should be:

$$E_d = \gamma_{sd} E \left\{ \gamma_{g,j} G_{k,j}; \gamma_p P; \gamma_{q,1} Q_{k,1}; \gamma_{q,i} \psi_{0,i} Q_{k,i} \right\} \quad j \geq 1; i > 1 \quad (6.9a)$$

(2) The combination of effects of actions to be considered should be based on

- the design value of the leading variable action, and
- the design combination values of accompanying variable actions :

Note: See also 6.4.3.2(4).

$$E_d = E \left\{ \gamma_{G,j} G_{k,j}; \gamma_p P; \gamma_{Q,1} Q_{k,1}; \gamma_{Q,i} \psi_{0,i} Q_{k,i} \right\} \quad j \geq 1; i > 1 \quad (6.9b)$$

(3) The combination of actions in brackets { }, in (6.9b) may either be expressed as:

$$\sum_{j \geq 1} \gamma_{G,j} G_{k,j} "+" \gamma_p P "+" \gamma_{Q,1} Q_{k,1} "+" \sum_{i > 1} \gamma_{Q,i} \psi_{0,i} Q_{k,i} \quad (6.10)$$

or, alternatively for STR and GEO limit states, the less favourable of the two following expressions:

$$\left\{ \sum_{j \geq 1} \gamma_{G,j} G_{k,j} "+" \gamma_p P "+" \gamma_{Q,1} \psi_{0,1} Q_{k,1} "+" \sum_{i > 1} \gamma_{Q,i} \psi_{0,i} Q_{k,i} \right. \quad (6.10a)$$

$$\left. \sum_{j \geq 1} \xi_j \gamma_{G,j} G_{k,j} "+" \gamma_p P "+" \gamma_{Q,1} Q_{k,1} "+" \sum_{i > 1} \gamma_{Q,i} \psi_{0,i} Q_{k,i} \right. \quad (6.10b)$$

Where :

"+" implies "to be combined with"

\sum implies "the combined effect of"

ξ is a reduction factor for unfavourable permanent actions G

Note: Further information for this choice is given in Annex A.

(4) If the relationship between actions and their effects is not linear, expressions (6.9a) or (6.9b) should be applied directly, depending upon the relative increase of the effects of actions compared to the increase in the magnitude of actions (see also 6.3.2.(4)).

6.4.3.3 Combinations of actions for accidental design situations

(1) The general format of effects of actions should be:

$$E_d = E \left\{ G_{k,j}; P; A_d; (\psi_{1,1} \text{ or } \psi_{2,1}) Q_{k,1}; \psi_{2,i} Q_{k,i} \right\} \quad j \geq 1; i > 1 \quad (6.11a)$$

(2) The combination of actions in brackets { } can be expressed as:

$$\sum_{j \geq 1} G_{k,j} \text{ "+" } P \text{ "+" } A_d \text{ "+" } (\psi_{1,1} \text{ or } \psi_{2,1}) Q_{k,1} \text{ "+" } \sum_{i > 1} \psi_{2,i} Q_{k,i} \quad (6.11b)$$

(3) The choice between $\psi_{1,1} Q_{k,1}$ or $\psi_{2,1} Q_{k,1}$ should be related to the relevant accidental design situation (impact, fire or survival after an accidental event or situation).

Note: Guidance is given in the relevant Parts of ES EN 1991:2015 to ES EN 1998:2015.

(4) Combinations of actions for accidental design situations should either

- involve an explicit accidental action A (fire or impact), or
- refer to a situation after an accidental event ($A = 0$).

For fire situations, apart from the temperature effect on the material properties, A_d should represent the design value of the indirect thermal action due to fire.

6.4.3.3 Combinations of actions for seismic design situations

(1) The general format of effects of actions should be:

$$E_d = E \left\{ G_{k,j}; P; A_{Ed}; \psi_{2,i} Q_{k,i} \right\} \quad j \geq 1; i \geq 1 \quad (6.12a)$$

(2) The combination of actions in brackets { } can be expressed as:

$$\sum_{j \geq 1} G_{k,j} \text{ "+" } P \text{ "+" } A_d \text{ "+" } \sum_{i \geq 1} \psi_{2,i} Q_{k,i} \quad (6.12b)$$

6.4.4 Partial factors for actions and combinations of actions

(1) The values of the γ and ψ factors for actions should be obtained from ES EN 1991:2015 and from Annex A.

6.4.5 Partial factors for materials and products

(1) The partial factors for properties of materials and products should be obtained from ES EN 1992:2015 to ES EN 1998:2015.

6.5 Serviceability limit states

6.5.1 Verifications

(1)P It shall be verified that :

$$E_d \leq C_d \quad (6.13)$$

where:

C_d is the limiting design value of the relevant serviceability criterion.

E_d is the design value of the effects of actions specified in the serviceability criterion, determined on the basis of the relevant combination.

6.5.2 Serviceability criteria

(1) The deformations to be taken into account in relation to serviceability requirements should be as detailed in the relevant Annex A according to the type of construction works, or agreed with the client or the National authority.

Note: For other specific serviceability criteria such as crack width, stress or strain limitation, slip resistance, see ES EN 1991:2015 to ES EN 1998:2015.

6.5.3 Combination of actions

(1) The combinations of actions to be taken into account in the relevant design situations should be appropriate for the serviceability requirements and performance criteria being verified.

(2) The combinations of actions for serviceability limit states are defined symbolically by the following expressions (see also 6.5.4):

Note: It is assumed, in these expressions, that all partial factors are equal to 1. See Annex A and ES EN 1991:2015 to ES EN 1998:2015.

a) Characteristic combination :

$$E_d = E \left\{ G_{k,j}; P; Q_{k,1}; \psi_{0,i} Q_{k,i} \right\} \quad j \geq 1; i > 1 \quad (6.14a)$$

in which the combination of actions in brackets { } (called the characteristic combination), can be expressed as:

$$\sum_{j \geq 1} G_{k,j} + P + Q_{k,1} + \sum_{i > 1} \psi_{0,i} Q_{k,i} \quad (6.14b)$$

Note: The characteristic combination is normally used for irreversible limit states.

b) Frequent combination:

$$E_d = E \left\{ G_{k,j}; P; \psi_{1,1} Q_{k,1}; \psi_{2,i} Q_{k,i} \right\} \quad j \geq 1; i > 1 \quad (6.15a)$$

in which the combination of actions in brackets { }, (called the frequent combination), can be expressed as:

$$\sum_{j \geq 1} G_{k,j} + P + \psi_{1,1} Q_{k,1} + \sum_{i > 1} \psi_{2,i} Q_{k,i} \quad (6.15b)$$

Note: The frequent combination is normally used for reversible limit states.

c) Quasi-permanent combination:

$$E_d = E \left\{ G_{k,j}; P; \psi_{2,i} Q_{k,i} \right\} \quad j \geq 1; i \geq 1 \quad (6.16a)$$

in which the combination of actions in brackets { }, (called the quasi-permanent combination), can be expressed as :

$$\sum_{j \geq 1} G_{k,j} + P + \sum_{i \geq 1} \psi_{2,i} Q_{k,i} \quad (6.16b)$$

where the notation is as given in 1.6 and 6.4.3(1).

Note: The quasi-permanent combination is normally used for long-term effects and the appearance of the structure.

(3) For the representative value of the prestressing action (i.e. P_k or P_m), reference should be made to the relevant design Ethiopian code for the type of prestress under consideration.

(4)P Effects of actions due to imposed deformations shall be considered where relevant.

Note: In some cases expressions (6.14) to (6.16) require modification. Detailed rules are given in the relevant Parts of ES EN 1991:2015 to ES EN 1998:2015.

6.5.4 Partial factors for materials

(1) For serviceability limit states the partial factors γ_M for the properties of materials should be taken as 1.0 except if differently specified in ES EN 1992:2015 to ES EN 1998:2015.

ANNEX A1
(INFORMATIVE)
APPLICATION FOR BUILDINGS

A1.1 Field of application

(1) This annex A1 gives rules and methods for establishing combinations of actions for buildings. It also gives the recommended design values of permanent, variable and accidental actions and ψ factors to be used in the design of buildings.

Note: Guidance may be given in the National annex with regard to the use of Table 2.1 (design working life).

A1.2 Combinations of actions**A1.2.1 General**

(1) Effects of actions that cannot exist simultaneously due to physical or functional reasons should not be considered together in combinations of actions.

Note 1: Depending on its uses and the form and the location of a building, the combinations of actions may be based on not more than two variable actions.

Note 2: Where modifications of A1.2.1(2) and A1.2.1(3) are necessary for geographical reasons, these can be defined in the National annex.

(2) The combinations of actions given in expressions 6.9a to 6.12b should be used when verifying ultimate limit states.

(3) The combinations of actions given in expressions 6.14a to 6.16b should be used when verifying serviceability limit states.

(4) Combinations of actions that include prestressing forces should be dealt with as detailed in ES EN 1992:2015 to ES EN 1998:2015.

A1.2.2 Values of ψ factors

(1) Values of ψ factors should be specified.

Note: Recommended values of ψ factors for the more common actions may be obtained from Table A1.1.

Table A1.1 - Recommended values of ψ factors for buildings

Action	ψ_0	ψ_1	ψ_2
Imposed loads in buildings, category (see ES EN 1991-1-1:2015)			
Category A : domestic, residential areas	0.7	0.5	0.3
Category B : office areas	0.7	0.5	0.3
Category C : congregation areas	0.7	0.7	0.6
Category D : shopping areas	0.7	0.7	0.6
Category E : storage areas	1.0	0.9	0.8
Category F : traffic area, vehicle weight $\leq 30\text{kN}$	0.7	0.7	0.6
Category G : traffic area $30\text{kN} < \text{vehicle weight} \leq 160\text{kN}$	0.7	0.5	0.3
Category H : roofs	0	0	0
Snow loads on buildings	0	0	0
Wind loads on buildings (see ES EN 1991-1-4:2015)	0.6	0.2	0
Temperature (non-fire) in buildings (see ES EN 1991-1-5:2015)	0.6	0.5	0

A1.3 Ultimate limit states

A1.3.1 Design values of actions in persistent and transient design situations

(1) The design values of actions for ultimate limit states in the persistent and transient design situations (expressions 6.9a to 6.10b) should be in accordance with Tables A1.2(A) to (C).

Note: The values in Tables A1.2 ((A) to (C)) can be altered e.g. for different reliability levels in the National annex (see Section 2 and Annex B).

(2) In applying Tables A1.2(A) to A1.2(C) in cases when the limit state is very sensitive to variations in the magnitude of permanent actions, the upper and lower characteristic values of actions should be taken according to 4.1.2(2)P.

(3) Static equilibrium (EQU, see 6.4.1) for building structures should be verified using the design values of actions in Table A1.2(A).

(4) Design of structural members (STR, see 6.4.1) not involving geotechnical actions should be verified using the design values of actions from Table A1.2(B).

(5) Design of structural members (footings, piles, basement walls, etc.) (STR) involving geotechnical actions and the resistance of the ground (GEO, see 6.4.1) should be verified using one of the following three approaches supplemented, for geotechnical actions and resistances, by ES EN 1997:2015 :

- Approach 1: Applying in separate calculations design values from Table A1.2(C) and Table A1.2(B) to the geotechnical actions as well as the other actions on/from the structure. In common cases, the sizing of foundations is governed by Table A1.2(C) and the structural resistance is governed by Table A1.2(B) ;

Note: In some cases, application of these tables is more complex, see ES EN 1997:2015.

- Approach 2: Applying design values from Table A1.2(B) to the geotechnical actions as well as the other actions on/from the structure ;
- Approach 3: Applying design values from Table A1.2(C) to the geotechnical actions and, simultaneously, applying partial factors from Table A1.2(B) to the other actions on/from the structure,

Note: The use of approaches 1, 2 or 3 is chosen in the National annex.

(6) Overall stability for building structures (e.g. the stability of a slope supporting a building) should be verified in accordance with ES EN 1997:2015.

(7) Hydraulic and buoyancy failure (e.g. in the bottom of an excavation for a building structure) should be verified in accordance with ES EN 1997:2015.

Table A1.2(A) - Design values of actions (EQU) (Set A)

Persistent and transient design situations	Permanent actions		Loading variable action (*)	Accompanying variable actions	
	Unfavorable	Favorable		Main (if any)	Others
(Eq.6.10)	$\gamma_{Gj,sup} G_{kj,sup}$	$\gamma_{Gj,inf} G_{kj,inf}$	$\gamma_{Q,1} Q_{k,1}$		$\gamma_{Q,i} \psi_{0,i} Q_{k,i}$

(*) Variable actions are those considered in Table A1.1

Note 1: The γ values may be set by the National annex. The recommended set of values for γ are:

$$\gamma_{G,j,sup} = 1.10$$

$$\gamma_{Gj,sup} = 0.90$$

$$\gamma_{Q,1} = 1.50 \text{ where unfavorable (0 where favorable)}$$

$$\gamma_{Q,i} = 1.50 \text{ where unfavorable (0 where favorable)}$$

Note 2: In cases where the verification of static equilibrium also involves the resistance of structural members, as an alternative to two separate verifications based on Table A1.2(A) and A1.2(B), a combined verification, based on Table A1.2(A), may be adopted, if allowed by the National annex, with the following set of recommend valves. The recommended values may be altered by the National annex.

$$\gamma_{Gj,sup} = 1.35$$

$$\gamma_{Gj,inf} = 1.15$$

$$\gamma_{Q,1} = 1.50 \text{ where unfavorable (0 where favorable)}$$

$$\gamma_{Q,i} = 1.50 \text{ where unfavorable (0 where favorable)}$$

Provided that applying $\gamma_{Gj,inf} = 1.00$ both to the favourable part and to the unfavorable part of permanent actions does not give a more unfavorable effect.

Table A1.2(B) - Design values of actions (STR/GEO) (Set B)

Persistent and transient design situations	Permanent actions		Leading variable action	Accompanying variable actions (*)		Persistent and transient design situations	Permanent actions		Leading variable action (*)	Accompanying variable actions (*)	
	Unfavourable	Favourable		Main (if any)	Others		Unfavourable	Favourable		Action	Main
(Eq.6.10)	$\gamma_{Gj,sup} G_{kj,sup}$	$\gamma_{Gj,inf} G_{kj,inf}$	$\gamma_{Q,1} Q_{k,1}$		$\gamma_{Q,i} \psi_{0,i} Q_{k,i}$	(Eq.6.10a)	$\gamma_{Gj,sup} G_{kj,sup}$	$\gamma_{Gj,inf} G_{kj,inf}$		$\gamma_{Q,1} \psi_{0,1} Q_{k,1}$	$\gamma_{Q,i} \psi_{0,i} Q_{k,i}$
						(Eq.6.10b)	$\xi \gamma_{Gj,sup} G_{kj,sup}$	$\gamma_{Gj,inf} G_{kj,inf}$	$\gamma_{Q,1} Q_{k,1}$		$\gamma_{Q,i} \psi_{0,i} Q_{k,i}$

(*) Variable actions are those considered in Table A1.1

Note 1: The choice between 6.10a and 6.10b will be in the National annex. In case of 6.10a and 6.10b, the National annex may in addition modify 6.10a to include permanent actions only.

Note 2: The γ and ξ values may be set by the National annex. The following values for γ and ξ are recommended when using expressions 6.10, or 6.10a and 6.10b.

$$\gamma_{Gj,sup} = 1.35$$

$$\gamma_{Gj,sup} = 1.00$$

$$\gamma_{Q,1} = 1.50 \text{ where unfavorable (0 where favorable)}$$

$$\gamma_{Q,i} = 1.50 \text{ where unfavorable (0 where favorable)}$$

$$\xi = 0.85 \text{ (so that } \xi \gamma_{Gj,sup} = 0.85 \times 1.35 \cong 1.15)$$

See also ES EN 1991:2015 to ES EN 1998:2015 for γ values to be used for imposed deformations.

Note 3: The characteristic values of all permanent actions from one source are multiplied by $\gamma_{G,sup}$ if the total resulting action effect is unfavourable and $\gamma_{G,inf}$ if the total resulting action effect is favourable. For example, all actions originating from the self weight of the structure may be considered as coming from one source; this also applies if different materials are involved.

Note 4: For particular verifications, the values for γ_G and γ_Q may be subdivided into γ_g and γ_q and the model uncertainty factor γ_{sd} in the range 1.05 to 1.15 can be used in most common cases and can be modified in the National annex.

Table A1.2(C) - Design values of actions (STR/GEO) (Set C)

Persistent and transient design situations	Permanent actions		Loading variable action (*)	Accompanying variable actions (*)	
	Unfavorable	Favorable		Main (if any)	Others
(Eq.6.10)	$\gamma_{Gj,sup} G_{kj,sup}$	$\gamma_{Gj,inf} G_{kj,inf}$	$\gamma_{Q,1} Q_{k,1}$		$\gamma_{Q,i} \psi_{0,i} Q_{k,i}$

(*) variable actions are those considered in Table A1.1

NOTE The γ values may be set by the National annex. The recommended set of values for γ are:

$\gamma_{Gj,sup} = 1.00$
 $\gamma_{Gj,inf} = 1.00$
 $\gamma_{Q,1} = 1.30$ where unfavorable (0 where favorable)
 $\gamma_{Q,i} = 1.30$ where unfavorable (0 where favorable)

A1.3.2 Design values of actions in the accidental and seismic design situations

(1) The partial factors for actions for the ultimate limit states in the accidental and seismic design situations (expressions 6.11a to 6.12b) should be 1.0. ψ values are given in Table A1.1.

Note: For the seismic design situation see also ES EN 1998:2015.

Table A1.3 - Design values of actions for use in accidental and seismic combinations of actions

Design situation	Permanent actions		Leading accidental or seismic action	Accompanying variable actions (**)	
	Unfavorable	Favorable		Main (if any)	Others
Accidental (*) (Eq. 6.11a/b)	$G_{kj,sup}$	$G_{kj,inf}$	A_d	ψ_{11} or ψ_{21} Q_{k1}	$\psi_{2,i} Q_{k,i}$
Seismic (Eq.6.12a/b)	$G_{kj,sup}$	$G_{kj,inf}$	$\gamma_1 A_{Ek}$ or A_{Ed}	$\psi_{2,i} Q_{k,i}$	

(*) In the case of accidental design situations, the main variable action may be taken with its frequent or, as in seismic combinations of actions, its quasi-permanent values. The choice will be in the National annex, depending on the accidental action under consideration. See also ES EN 1991-1-2:2015.

(**) Variable actions are those considered in Table A1.1

A1.4 Serviceability limit states

A1.4.1 Partial factors for actions

(1) For serviceability limit states the partial factors for actions should be taken as 1.0 except if differently specified in ES EN 1991:2015 to ES EN 1998:2015.

Table A1.4 - Design values of actions for use in the combination of actions

Combination	Permanent actions G_d		Variable actions Q_d	
	Unfavourable	Favorable	Leading	Others
Characteristic	$G_{kj,sup}$	$G_{kj,inf}$	$Q_{k,1}$	$\psi_{0,i} Q_{k,i}$
Frequent	$G_{kj,sup}$	$G_{kj,inf}$	$\psi_{1,1} Q_{k,1}$	$\psi_{2,i} Q_{k,i}$
Quasi-permanent	$G_{kj,sup}$	$G_{kj,inf}$	$\psi_{2,1} Q_{k,1}$	$\psi_{2,i} Q_{k,i}$

A1.4.2 Serviceability criteria

(1) Serviceability limit states in buildings should take into account criteria related, for example, to floor stiffness, differential floor levels, storey sway or/and building sway and roof stiffness. Stiffness criteria may be expressed in terms of limits for vertical deflections and for vibrations. Sway criteria may be expressed in terms of limits for horizontal displacements.

(2) The serviceability criteria should be specified for each project and agreed with the client.

Note : The serviceability criteria may be defined in the National annex.

(3) P The serviceability criteria for deformations and vibrations shall be defined:

- depending on the intended use;
- in relation to the serviceability requirements in accordance with 3.4 ;
- independently of the materials used for supporting structural member.

A1.4.3 Deformations and horizontal displacements

(1) Vertical and horizontal deformations should be calculated in accordance with ES EN 1992:2015 to ES EN 1998:2015, by using the appropriate combinations of actions according to expressions (6.14a) to (6.16b) taking into account the serviceability requirements given in 3.4(1). Special attention should be given to the distinction between reversible and irreversible limit states.

(2) Vertical deflections are represented schematically in Figure. A1.1.

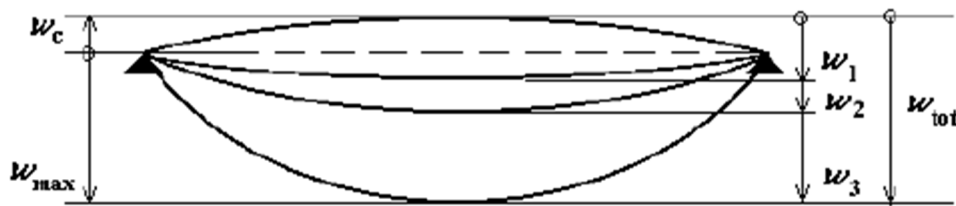


Figure A1.1 - Definitions of vertical deflections

Key :

- w_c Precamber in the unloaded structural member
- w_1 Initial part of the deflection under permanent loads of the relevant combination of actions according to expressions (6.14a) to (6.16b)
- w_2 Long-term part of the deflection under permanent loads
- w_3 Additional part of the deflection due to the variable actions of the relevant combination of actions according to expressions (6.14a) to (6.16b)
- w_{tot} Total deflection as sum of w_1 , w_2 , w_3
- w_{max} Remaining total deflection taking into account the precamber

(3) If the functioning or damage of the structure or to finishes, or to non-structural members (e.g. partition walls, claddings) is being considered, the verification for deflection should take account of those effects of permanent and variable actions that occur after the execution of the member or finish concerned.

Note: Guidance on which expression (6.14a) to (6.16b) to use is given in 6.5.3 and ES EN 1992:2015 to ES EN 1998:2015.

(4) If the appearance of the structure is being considered, the quasi-permanent combination (expression 6.16b) should be used.

(5) If the comfort of the user or the functioning of machinery are being considered, the verification should take account of the effects of the relevant variable actions.

(6) Long term deformations due to shrinkage, relaxation or creep should be considered where relevant, and calculated by using the effects of the permanent actions and quasi-permanent values of the variable actions.

(7) Horizontal displacements are represented schematically in Figure A1.2.

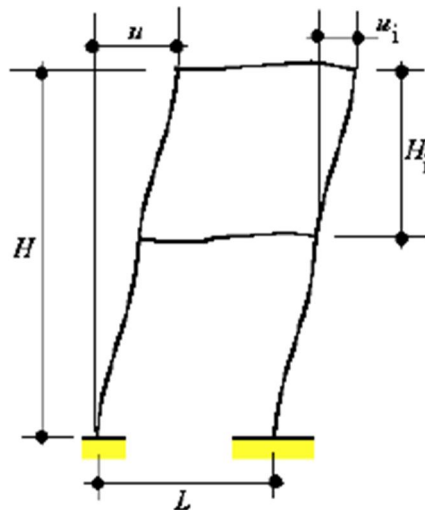


Figure A1.2 - Definition of horizontal displacements

Key :

- u Overall horizontal displacement over the building height H
- u_i Horizontal displacement over a storey height H_i

A1.4.4 Vibrations

(1) To achieve satisfactory vibration behaviour of buildings and their structural members under serviceability conditions, the following aspects, amongst others, should be considered :

- a) the comfort of the user;
- b) the functioning of the structure or its structural members (e.g. cracks in partitions, damage to cladding, sensitivity of building contents to vibrations).

Other aspects should be considered for each project and agreed with the client.

(2) For the serviceability limit state of a structure or a structural member not to be exceeded when subjected to vibrations, the natural frequency of vibrations of the structure or structural member should be kept above appropriate values which depend upon the function of the building and the source of the vibration, and agreed with the client and/or the relevant authority.

(3) If the natural frequency of vibrations of the structure is lower than the appropriate value, a more refined analysis of the dynamic response of the structure, including the consideration of damping, should be performed.

Note: For further guidance, see ES N 1991-1-1:2015, ES EN 1991-1-4:2015 and ES ISO 10137.

(4) Possible sources of vibration that should be considered include walking, synchronised movements of people, machinery, ground borne vibrations from traffic, and wind actions. These, and other sources, should be specified for each project and agreed with the client.

ANNEX B
(INFORMATIVE)
MANAGEMENT OF STRUCTURAL RELIABILITY FOR CONSTRUCTION WORKS

B1 Scope and field of application

(1) This annex provides additional guidance to 2.2 (Reliability management) and to appropriate clauses in ES EN 1991:2015 to ES EN 1998:2015.

Note: Reliability differentiation rules have been specified for particular aspects in the design ESs, e.g. in ES EN 1992:2015, ES EN 1993:2015, ES EN 1996:2015, ES EN 1997:2015 and ES EN 1998:2015.

(2) The approach given in this Annex recommends the following procedures for the management of structural reliability for construction works (with regard to ULSs, excluding fatigue):

a) In relation to 2.2(5)b, classes are introduced and are based on the assumed consequences of failure and the exposure of the construction works to hazard. A procedure for allowing moderate differentiation in the partial factors for actions and resistances corresponding to the classes is given in B3.

Note: Reliability classification can be represented by β indexes (see Annex C) which takes account of accepted or assumed statistical variability in action effects and resistances and model uncertainties.

b) In relation to 2.2(5)c and 2.2(5)d, a procedure for allowing differentiation between various types of construction works in the requirements for quality levels of the design and execution process are given in B4 and B5.

Note: Those quality management and control measures in design, detailing and execution which are given in B4 and B5 aim to eliminate failures due to gross errors, and ensure the resistances assumed in the design.

(3) The procedure has been formulated in such a way so as to produce a framework to allow different reliability levels to be used, if desired.

B2 Symbols

In this annex the following symbols apply.

K_{FI}	Factor applicable to actions for reliability differentiation
β	Reliability index

B3 Reliability differentiation

B3.1 Consequences classes

(1) For the purpose of reliability differentiation, consequences classes (CC) may be established by considering the consequences of failure or malfunction of the structure as given in Table B1.

Table B1 - Definition of consequences classes

Consequences Class	Description	Examples of buildings and civil engineering works
CC3	High consequence for loss of human life, or economic, social or environmental consequences very great	Grandstands, public buildings where consequences of failure are high (e.g. a concert hall)
CC2	Medium consequence for loss of human life, economic, social or environmental consequences considerable	Residential and office buildings, public buildings where consequences of failure are medium (e.g. an office building)
CC1	Low consequence for loss of human life, <i>and</i> economic, social or environmental consequences small or negligible	Agricultural buildings where people do not normally enter (e.g. storage buildings), greenhouses

(2) The criterion for classification of consequences is the importance, in terms of consequences of failure, of the structure or structural member concerned. See B3.3

(3) Depending on the structural form and decisions made during design, particular members of the structure may be designated in the same, higher or lower consequences class than for the entire structure.

Note: At the present time the requirements for reliability are related to the structural members of the construction works.

B3.2 Differentiation by β values

(1) The reliability classes (RC) may be defined by the β reliability index concept.

(2) Three reliability classes RC1, RC2 and RC3 may be associated with the three consequences classes CC1, CC2 and CC3.

(3) Table B2 gives recommended minimum values for the reliability index associated with reliability classes (see also annex C).

Table B2 - Recommended minimum values for reliability index β (ultimate limit states)

Reliability Class	Minimum values for β	
	1 year reference period	50 years reference period
RC3	5.2	4.3
RC2	4.7	3.8
RC1	4.2	3.3

Note: A design using ES EN 1990:2015 with the partial factors given in annex A1 and ES EN 1991:2015 to ES EN 1998:2015 is considered generally to lead to a structure with a β value greater than 3.8 for a 50 year reference period. Reliability classes for members of the structure above RC3 are not further considered in this Annex, since these structures each require individual consideration.

B3.3 Differentiation by measures relating to the partial factors

(1) One way of achieving reliability differentiation is by distinguishing classes of γ_F factors to be used in fundamental combinations for persistent design situations. For example, for the same design supervision and execution inspection levels, a multiplication factor K_{FI} , see Table B3, may be applied to the partial factors.

Table B3 - K_{FI} factor for actions

K_{FI} factor for actions	Reliability class		
	RC1	RC2	RC3
K_{FI}	0.9	1.0	1.1

Note: In particular, for class RC3, other measures as described in this Annex are normally preferred to using K_{FI} factors. K_{FI} should be applied only to unfavourable actions.

(2) Reliability differentiation may also be applied through the partial factors on resistance γ_M . However, this is not normally used. An exception is in relation to fatigue verification (see ES EN 1993:2015). See also B6.

(3) Accompanying measures, for example the level of quality control for the design and execution of the structure, may be associated to the classes of γ_F . In this Annex, a three level system for control during design and execution has been adopted. Design supervision levels and inspection levels associated with the reliability classes are suggested.

(4) There can be cases (e.g. lighting poles, masts, etc.) where, for reasons of economy, the structure might be in RC1, but be subjected to higher corresponding design supervision and inspection levels.

B4 Design supervision differentiation

(1) Design supervision differentiation consists of various organisational quality control measures which can be used together. For example, the definition of design supervision level (B4(2)) may be used together with other measures such as classification of designers and checking authorities (B4(3)).

(2) Three possible design supervision levels (DSL) are shown in Table B4. The design supervision levels may be linked to the reliability class selected or chosen according to the importance of the structure and in accordance with National requirements or the design brief, and implemented through appropriate quality management measures. See 2.5.

Table B4 - Design supervision levels (DSL)

Design Supervision Levels	Characteristics	Minimum recommended requirements for checking of calculations, drawings and specifications
DSL3 relating to RC3	Extended supervision	Third party checking: Checking performed by an organization different from that which has prepared the design
DSL2 relating to RC2	Normal supervision	Checking by different persons than those originally responsible and in accordance with the procedure of the organization.
DSL1 relating to RC1	Normal supervision	Self-checking: Checking performed by the person who has prepared the design

(3) Design supervision differentiation may also include a classification of designers and/or design inspectors (checkers, controlling authorities, etc.), depending on their competence and experience, their internal organisation, for the relevant type of construction works being designed.

Note: The type of construction works, the materials used and the structural forms can affect this classification.

(4) Alternatively, design supervision differentiation can consist of a more refined detailed assessment of the nature and magnitude of actions to be resisted by the structure, or of a system of design load management to actively or passively control (restrict) these actions.

B5 Inspection during execution

(1) Three inspection levels (IL) may be introduced as shown in Table B5. The inspection levels may be linked to the quality management classes selected and implemented through appropriate quality management measures. See 2.5. Further guidance is available in relevant execution standards referenced by ES EN 1992:2015 to ES EN 1996:2015.

Table B5 - Inspection levels (IL)

Inspection Levels	Characteristics	Requirements
IL3 Relating to RC3	Extended inspection	Third party inspection
IL2 Relating to RC2	Normal inspection	Inspection in accordance with the procedures of the organization
IL1 Relating to RC1	Normal inspection	Self inspection

Note: Inspection levels define the subjects to be covered by inspection of products and execution of works including the scope of inspection. The rules will thus vary from one structural material to another, and are to be given in the relevant execution standards.

B6 Partial factors for resistance properties

(1) A partial factor for a material or product property or a member resistance may be reduced if an inspection class higher than that required according to Table B5 and/or more severe requirements are used.

Note: For verifying efficiency by testing see section 5 and Annex D.

Note: Rules for various materials may be given or referenced in ES EN 1992:2015 to ES EN 1998:2015.

Note: Such a reduction, which allows for example for model uncertainties and dimensional variation, is not a reliability differentiation measure: it is only a compensating measure in order to keep the reliability level dependent on the efficiency of the control measures.

ANNEX C
(INFORMATIVE)

BASIS FOR PARTIAL FACTOR DESIGN AND RELIABILITY ANALYSIS

C1 Scope and Field of Applications

(1) This annex provides information and theoretical background to the partial factor method described in Section 6 and annex A. This Annex also provides the background to annex D, and is relevant to the contents of annex B.

(2) This annex also provides information on

- the structural reliability methods ;
- the application of the reliability-based method to determine by calibration design values and/or partial factors in the design expressions ;
- the design verification formats in the ES.

C2 Symbols

In this annex the following symbols apply.

Latin upper case letters

P_f	Failure probability
Prob(.)	Probability
P_s	survival probability

Latin lower case letters

a	geometrical property
g	<i>performance function</i>

Greek upper case letters

Φ	<i>cumulative distribution function of the standardised Normal distribution</i>
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Greek lower case letters

α_E	FORM (First Order Reliability Method) sensitivity factor for effects of actions
α_R	FORM (First Order Reliability Method) sensitivity factor for resistance
β	reliability index
θ	model uncertainty
μ_x	mean value of X
σ_x	standard deviation of X
V_x	coefficient of variation of X

C3 Introduction

(1) In the partial factor method the basic variables (i.e. actions, resistances and geometrical properties) through the use of partial factors and ψ factors are given design values, and a verification made to ensure that no relevant limit state has been exceeded. See C7.

Note: Section 6 describes the design values for actions and the effects of actions, and design values of material and product properties and geometrical data.

(2) In principle numerical values for partial factors and ψ factors can be determined in either of two ways :

a) On the basis of calibration to a long experience of building tradition.

Note: For most of the partial factors and the ψ factors proposed in the currently available ES this is the leading Principle.

b) On the basis of statistical evaluation of experimental data and field observations. (This should be carried out within the framework of a probabilistic reliability theory.)

(3) When using method 2b), either on its own or in combination with method 2a), ultimate limit states partial factors for different materials and actions should be calibrated such that the reliability levels for representative structures are as close as possible to the target reliability index. See C6.

C4 Overview of reliability methods

(1) Figure C1 presents a diagrammatic overview of the various methods available for calibration of partial factor (limit states) design equations and the relation between them.

(2) The probabilistic calibration procedures for partial factors can be subdivided into two main classes :

- full probabilistic methods (Level III), and
- first order reliability methods (FORM) (Level II).

Note 1: Full probabilistic methods (Level III) give in principle correct answers to the reliability problem as stated. Level III methods are seldom used in the calibration of design codes because of the frequent lack of statistical data.

Note 2: The level II methods make use of certain well defined approximations and lead to results which for most structural applications can be considered sufficiently accurate.

(3) In both the Level II and Level III methods the measure of reliability should be identified with the survival probability $P_s = (1 - P_f)$, where P_f is the failure probability for the considered failure mode and within an appropriate reference period. If the calculated

failure probability is larger than a pre-set target value P_0 , then the structure should be considered to be unsafe.

Note: The 'probability of failure' and its corresponding reliability index (see C5) are only notional values that do not necessarily represent the actual failure rates but are used as operational values for code calibration purposes and comparison of reliability levels of structures.

(4) The ES have been primarily based on method *a* (see Figure C1). Method *c* or equivalent methods have been used for further development of the ES.

Note: An example of an equivalent method is design assisted by testing (see annex D).

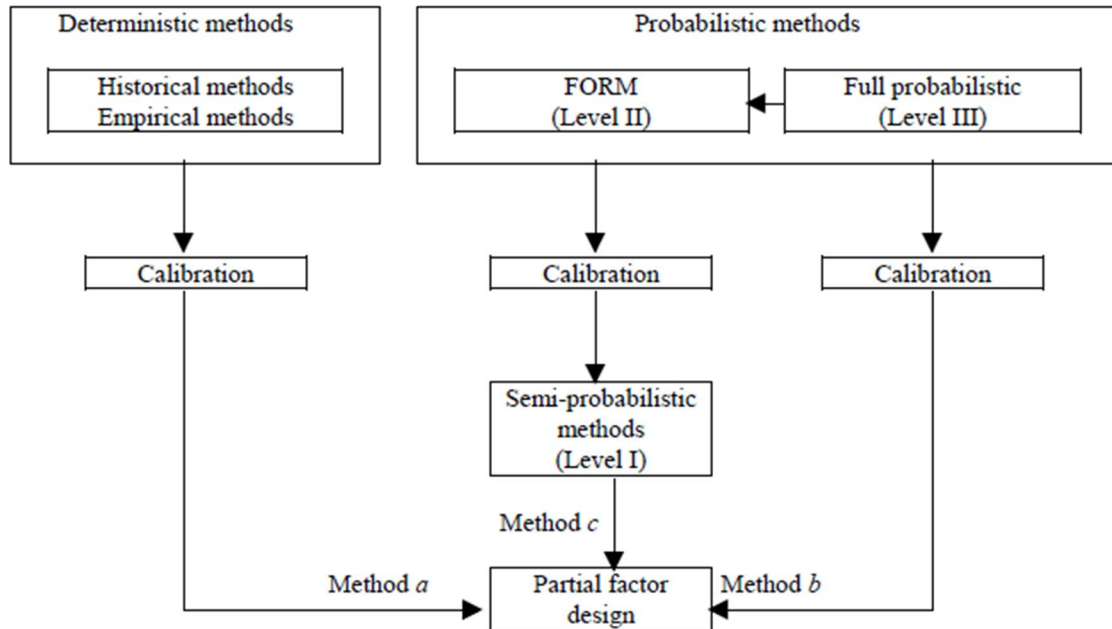


Figure C1 - Overview of reliability methods

C5 Reliability index β

(1) In the Level II procedures, an alternative measure of reliability is conventionally defined by the reliability index β which is related to P_f by:

$$P_f = \Phi(-\beta) \tag{C.1}$$

where Φ is the cumulative distribution function of the standardised Normal distribution. The relation between Φ and β is given in Table C1.

Table C1 - Relation between β and P_f

P_f	10^{-1}	10^{-2}	10^{-3}	10^{-4}	10^{-5}	10^{-6}	10^{-7}
β	1.28	2.32	3.09	3.72	4.27	4.75	5.20

(2) The probability of failure P_f can be expressed through a performance function g such that a structure is considered to survive if $g > 0$ and to fail if $g \leq 0$:

$$P_f = \text{Prob}(g \leq 0) \tag{C.2a}$$

If R is the resistance and E the effect of actions, the performance function g is :

$$g = R - E \tag{C.2b}$$

with R , E and g random variables.

(3) If g is Normally distributed, β is taken as :

$$\beta = \frac{\mu_g}{\sigma_g} \quad (\text{C.2c})$$

where :

μ_g is the mean value of g , and

σ_g is its standard deviation,

so that :

$$\mu_g - \beta\sigma_g = 0 \quad (\text{C.2d})$$

and

$$P_f = \text{Prob}(g \leq 0) = P_f = \text{Prob}(g \leq \mu_g - \beta\sigma_g) \quad (\text{C.2e})$$

For other distributions of g , β is only a conventional measure of the reliability

$$P_s = (1 - P_f)$$

C6 Target values of reliability index β

(1) Target values for the reliability index β for various design situations, and for reference periods of 1 year and 50 years, are indicated in Table C2. The values of β in Table C2 correspond to levels of safety for reliability class RC2 (see Annex B) structural members.

Note 1: For these evaluations of β

- Lognormal or Weibull distributions have usually been used for material and structural resistance parameters and model uncertainties;
- Normal distributions have usually been used for self-weight;
- For simplicity, when considering non-fatigue verifications, Normal distributions have been used for variable actions. Extreme value distributions would be more appropriate.

Note 2: When the main uncertainty comes from actions that have statistically independent maxima in each year, the values of β for a different reference period can be calculated using the following expression

$$\Phi(\beta_n) = [\Phi(\beta_1)]^n \quad (\text{C.3})$$

where :

β_n is the reliability index for a reference period of n years,

β_1 is the reliability index for one year.

Table C2 - Target reliability index β for Class RC2 structural members ¹⁾

Limit state	Target reliability index	
	1 year	50 years
Ultimate	4.7	3.8
Fatigue		1.5 to 3.8 ²⁾
Serviceability (irreversible)	2.9	1.5
¹⁾ See Annex B		
²⁾ Depends on degree of inspectability, reparability and damage tolerance.		

(2) The actual frequency of failure is significantly dependent upon human error, which are not considered in partial factor design (See Annex B). Thus β does not necessarily provide an indication of the actual frequency of structural failure.

C7 Approach for calibration of design values

(1) In the design value method of reliability verification (see Figure C1), design values need to be defined for all the basic variables. A design is considered to be sufficient if the limit states are not reached when the design values are introduced into the analysis models. In symbolic notation this is expressed as :

$$E_d < R_d \quad (C.4)$$

where the subscript 'd' refers to design values. This is the practical way to ensure that the reliability index β is equal to or larger than the target value.

E_d and R_d can be expressed in partly symbolic form as :

$$E_d = E \{ F_{d1}, F_{d2} \dots a_{d1}, a_{d2} \dots \theta_{d1}, \theta_{d2}, \dots \} \quad (C.5a)$$

$$R_d = R \{ X_{d1}, X_{d2} \dots a_{d1}, a_{d2} \dots \theta_{d1}, \theta_{d2}, \dots \} \quad (C.5b)$$

where :

- E is the action effect ;
- R is the resistance ;
- F is an action ;
- X is a material property ;
- a is a geometrical property ;
- θ is a model uncertainty.

For particular limit states (e.g. fatigue) a more general formulation may be necessary to express a limit state.

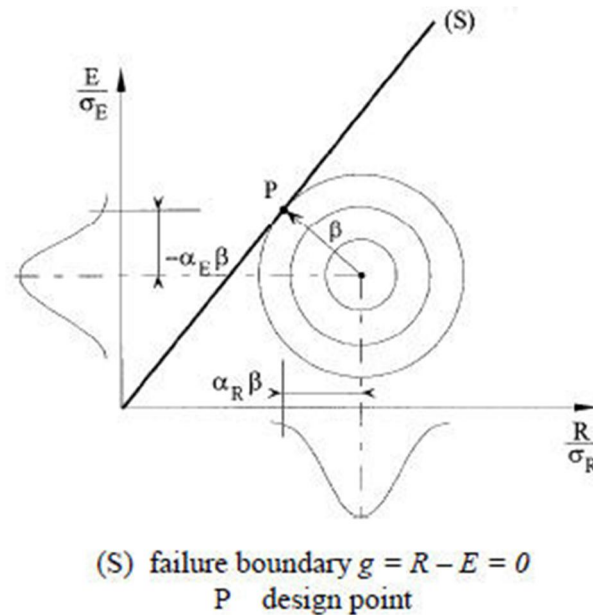


Figure C2 - Design point and reliability index β according to the first order reliability method (FORM) for Normally distributed uncorrelated variables

(2) Design values should be based on the values of the basic variables at the FORM design point, which can be defined as the point on the failure surface ($g = 0$) closest to the average point in the space of normalised variables (as diagrammatically indicated in Figure C2).

(3) The design values of action effects E_d and resistances R_d should be defined such that the probability of having a more unfavourable value is as follows :

$$P(E > E_d) = \Phi(+\alpha_E \beta) \quad (\text{C.6a})$$

$$P(R \leq R_d) = \Phi(-\alpha_R \beta) \quad (\text{C.6b})$$

where :

β is the target reliability index (see C6).

α_E and α_R , with $|\alpha| \leq 1$, are the values of the FORM sensitivity factors. The value of α is negative for unfavourable actions and action effects, and positive for resistances.

α_E and α_R may be taken as -0.7 and 0.8 , respectively, provided

$$0.16 < \sigma_E / \sigma_R < 7.6 \quad (\text{C.7})$$

where σ_E and σ_R are the standard deviations of the action effect and resistance, respectively, in expressions (C.6a) and (C.6b). This gives :

$$P(E > E_d) = \Phi(-0.7\beta) \tag{C.8a}$$

$$P(R \leq R_d) = \Phi(-0.8\beta) \tag{C.8b}$$

(4) Where condition (C.7) is not satisfied $\alpha = \pm 1.0$ should be used for the variable with the larger standard deviation, and $\alpha = \pm 0.4$ for the variable with the smaller standard deviation.

(5) When the action model contains several basic variables, expression (C.8a) should be used for the leading variable only. For the accompanying actions the design values may be defined by :

$$P(E > E_d) = \Phi(-0.4 \times 0.7x\beta) = \Phi(-0.28\beta) \tag{C.9}$$

Note: For $\beta = 3.8$ the values defined by expression (C.9) correspond approximately to the 0.90 fractile.

(6) The expressions provided in Table C3 should be used for deriving the design values of variables with the given probability distribution.

Table C3 - Design values for various distribution functions

Distribution	Design values
Normal	$\mu - \alpha\beta\sigma$
Lognormal	$\mu \exp(-\alpha\beta V)$ for $V = \sigma / \mu < 0.2$
Gumbel	$u - \frac{1}{a} \ln \{ -\ln \Phi(-\alpha\beta) \}$ <p>where $u = \mu - \frac{0.577}{a}$; $a = \frac{\pi}{\sigma\sqrt{6}}$</p>

Note: In these expressions μ , σ and V are, respectively, the mean value, the standard deviation and the coefficient of variation of a given variable. For variable actions, these should be based on the same reference period as for β

(7) One method of obtaining the relevant partial factor is to divide the design value of a variable action by its representative or characteristic value.

C8 Reliability verification formats in ES

(1) In ES EN 1990:2015 to ES EN 1998:2015, the design values of the basic variables, X_d and F_d , are usually not introduced directly into the partial factor design equations. They are introduced in terms of their representative values X_{rep} and F_{rep} , which may be :

- characteristic values, i.e. values with a prescribed or intended probability of being exceeded, e.g. for actions, material properties and geometrical properties (see 1.5.3.14, 1.5.4.1 and 1.5.5.1, respectively) ;
- nominal values, which are treated as characteristic values for material properties (see 1.5.4.3) and as design values for geometrical properties (see 1.5.5.2).

(2) The representative values X_{rep} and F_{rep} , should be divided and/or multiplied, respectively, by the appropriate partial factors to obtain the design values X_d and F_d

Note: See also expression (C.10).

(3) Design values of actions F , material properties X and geometrical properties a are given in expressions (6.1), (6.3) and (6.4), respectively.

Where an upper value for design resistance is used (see 6.3.3), the expression (6.3) takes the form :

$$X_d = \eta \gamma_{fM} X_{k,sup} \quad (C.10)$$

where γ_{fM} is an appropriate factor greater than 1.

Note: Expression (C.10) may be used for capacity design.

(4) Design values for model uncertainties may be incorporated into the design expressions through the partial factors γ_{Sd} and γ_{Rd} applied on the total model, such that :

$$E_d = \gamma_{Sd} E \{ \gamma_{gj} G_{kj}; \gamma_P P; \gamma_{q1} Q_{k1}; \gamma_{qi} \psi_{0i} Q_{ki}; a_d \dots \} \quad (C.11)$$

$$R_d = R \{ \eta X_k / \gamma_m; a_d \dots \} / \gamma_{Rd} \quad (C.12)$$

(5) The coefficient ψ which takes account of reductions in the design values of variable actions, is applied as ψ_0 , ψ_1 or ψ_2 to simultaneously occurring, accompanying variable actions.

(6) The following simplifications may be made to expression (C.11) and (C.12), when required.

a) On the loading side (for a single action or where linearity of action effects exists):

$$Ed = E \{ \gamma_{F,i} F_{rep,i}; a_d \} \quad (C.13)$$

b) On the resistance side the general format is given in expressions (6.6), and further simplifications may be given in the relevant material ES. The simplifications should only be made if the level of reliability is not reduced.

Note: Non-linear resistance and actions models, and multi-variable action or resistance models, are commonly encountered in ES. In such instances, the above relations become more complex.

C9 Partial factors in ES EN 1990:2015

- (1) The different partial factors available in ES EN 1990:2015 are defined in 1.6.
- (2) The relation between individual partial factors in ES is schematically shown Figure C3.

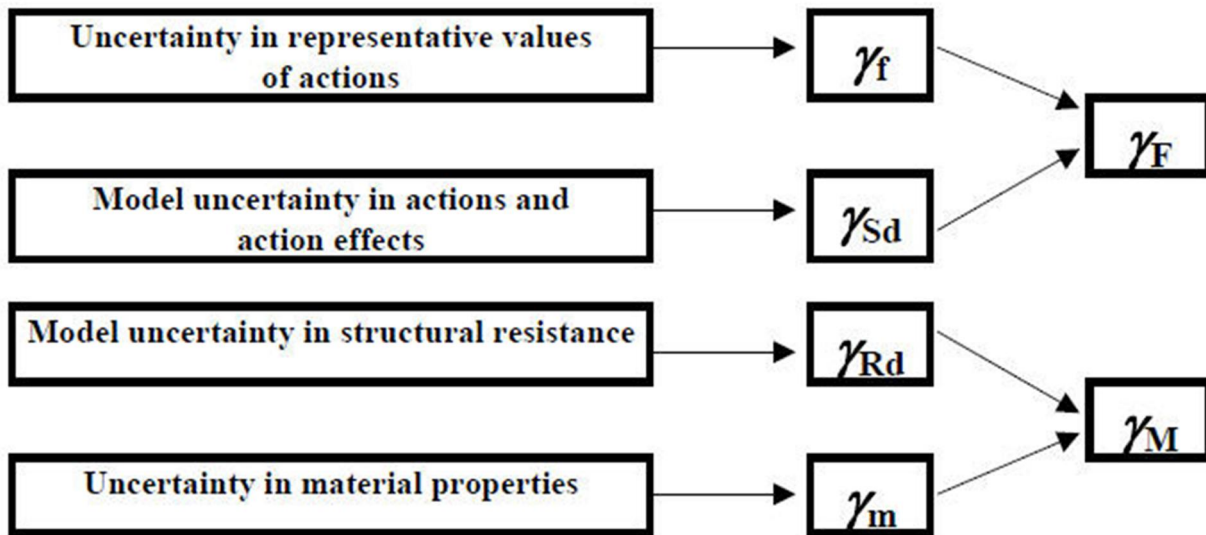


Figure C3 - Relation between individual partial factors

C10 ψ_0 factors

- (1) Table C4 gives expressions for obtaining the ψ_0 factors (see Section 6) in the case of two variable actions.
- (2) The expressions in Table C4 have been derived by using the following assumptions and conditions :
- the two actions to be combined are independent of each other ;
 - the basic period (T_1 or T_2) for each action is constant ; T_1 is the greater basic period ;
 - the action values within respective basic periods are constant ;
 - the intensities of an action within basic periods are uncorrelated ;
 - the two actions belong to ergodic processes.
- (3) The distribution functions in Table C4 refer to the maxima within the reference period T . These distribution functions are total functions which consider the probability that an action value is zero during certain periods.

Table C4 - Expressions for ψ_0 for the case of two variable actions

Distribution	$\psi_0 = F_{\text{accompanying}} / F_{\text{leading}}$
General	$\frac{F_s^{-1} \{ \Phi(0.4\beta')^{N_1} \}}{F_s^{-1} \{ \Phi(0.7\beta)^{N_1} \}}$ <p>with $\beta' = -\Phi^{-1} \{ \Phi(-0.7\beta) / N_1 \}$</p>
Approximation for very large N_1	$\frac{F_s^{-1} \left\{ \exp \left[-N_1 \Phi(-0.4\beta') \right] \right\}}{F_s^{-1} \{ \Phi(0.7\beta) \}}$ <p>with $\beta' = -\Phi^{-1} \{ \Phi(-0.7\beta) / N_1 \}$</p>
Normal (approximation)	$\frac{1 + (0.28\beta - 0.7 \ln N_1)V}{1 + 0.7\beta V}$
Gumbel (approximation)	$\frac{1 - 0.78V \left[0.58 + \ln(-\ln \Phi(0.28\beta)) + \ln N_1 \right]}{1 - 0.78V \left[0.58 + \ln(-\ln \Phi(0.7\beta)) \right]}$
<p>$F_s(.)$ is the probability distribution function of the extreme value of the accompanying action in the reference period T ; $\Phi(.)$ is the standard Normal distribution function; T is the reference period; T_1 is the greater of the basic periods for actions to be combined; N_1 is the ratio T/T_1, approximated to the nearest integer; β is the reliability index ; V is the coefficient of variation of the accompanying action for the reference period.</p>	

ANNEX D
(INFORMATIVE)
DESIGN ASSISTED BY TESTING

D1 Scope and field of application

- (1) This annex provides guidance on 3.4, 4.2 and 5.2.
- (2) This annex is not intended to replace product specifications or execution standards.

D2 Symbols

In this annex, the following symbols apply.

Latin upper case letters

$E(.)$	Mean value of (.)
V	Coefficient of variation [$V = (\text{standard deviation}) / (\text{mean value})$]
V_X	Coefficient of variation of X
V_δ	Estimator for the coefficient of variation of the error term δ
\underline{X}	Array of j basic variables $X_1 \dots X_j$
$X_{k(n)}$	Characteristic value, including statistical uncertainty for a sample of size n with any conversion factor excluded
\underline{X}_m	Array of mean values of the basic variables
\underline{X}_n	Array of nominal values of the basic variables

Latin lower case letters

b	Correction factor
b_i	Correction factor for test specimen i
$g_r(\underline{X})$	Resistance function (of the basic variables \underline{X}) used as the design model
$k_{d,n}$	Design fractile factor
k_n	Characteristic fractile factor
m_X	Mean of the n sample results
n	Number of experiments or numerical test results
r	Resistance value
r_d	Design value of the resistance
r_e	Experimental resistance value
r_{ee}	Extreme (maximum or minimum) value of the experimental resistance [i.e. value of r_e that deviates most from the mean value r_{em}]
r_{ei}	Experimental resistance for specimen i
r_{em}	Mean value of the experimental resistance
r_k	Characteristic value of the resistance
r_m	Resistance value calculated using the mean values \underline{X}_m of the basic variables

r_n	Nominal value of the resistance
r_t	Theoretical resistance determined from the resistance function $g_r(\underline{X})$
r_{ti}	Theoretical resistance determined using the measured parameters \underline{X} for specimen i
s	Estimated value of the standard deviation σ
s_Δ	Estimated value of σ_Δ
s_δ	Estimated value of σ_δ

Greek upper case letters

Φ	Cumulative distribution function of the standardised Normal distribution
Δ	Logarithm of the error term $\delta [\Delta_i = \ln(\delta_i)]$
$\bar{\Delta}$	Estimated value for $E(\Delta)$

Greek lower case letters

α_E	FORM (First Order Reliability Method) sensitivity factor for effects of actions
α_R	FORM (First Order Reliability Method) sensitivity factor for resistance
β	Reliability index
γ_M^*	Corrected partial factor for resistances [$\gamma_M^* = r_n / r_d$ so $\gamma_M^* = k_c \gamma_M$]
δ	Error term
δ_i	Observed error term for test specimen i obtained from a comparison of the experimental resistance r_{ei} and the mean value corrected theoretical resistance br_{ti}
η_d	Design value of the possible conversion factor (so far as is not included in partial factor for resistance γ_M)
η_k	Reduction factor applicable in the case of prior knowledge
σ	Standard deviation [$\sigma = \sqrt{\text{variance}}$]
σ_Δ^2	Variance of the term

D3 Types of tests

(1) A distinction needs to be made between the following types of tests:

a) tests to establish directly the ultimate resistance or serviceability properties of structures or structural members for given loading conditions. Such tests can be performed, for example, for fatigue loads or impact loads;

b) tests to obtain specific material properties using specified testing procedures ; for instance, ground testing in situ or in the laboratory, or the testing of new materials ;

c) tests to reduce uncertainties in parameters in load or load effect models; for instance, by wind tunnel testing, or in tests to identify actions from waves or currents ;

d) tests to reduce uncertainties in parameters used in resistance models ; for instance, by testing structural members or assemblies of structural members (e.g. roof or floor structures) ;

e) control tests to check the identity or quality of delivered products or the consistency of production characteristics ; for instance, testing of cables for bridges, or concrete cube testing ;

f) tests carried out during execution in order to obtain information needed for part of the execution ; for instance, testing of pile resistance, testing of cable forces during execution ;

g) control tests to check the behaviour of an actual structure or of structural members after completion, e.g. to find the elastic deflection, vibrational frequencies or damping ;

(2) For test types (a), (b), (c), (d), the design values to be used should wherever practicable be derived from the test results by applying accepted statistical techniques. See D5 to D8.

Note: Special techniques might be needed in order to evaluate type (c) test results.

(3) Test types (e), (f), (g) may be considered as acceptance tests where no test results are available at the time of design. Design values should be conservative estimates which are expected to be able to meet the acceptance criteria (tests (e), (f), (g)) at a later stage.

D4 Planning of tests

(1) Prior to the carrying out of tests, a test plan should be agreed with the testing organization. This plan should contain the objectives of the test and all specifications necessary for the election or production of the test specimens, the execution of the tests and the test evaluation. The test plan should cover :

- objectives and scope,
- prediction of test results,
- specification of test specimens and sampling,
- loading specifications,
- testing arrangement,
- measurements,
- evaluation and reporting of the tests.

Objectives and scope: The objective of the tests should be clearly stated, e.g. the required properties, the influence of certain design parameters varied during the test and the range of validity. Limitations of the test and required conversions (e.g. scaling effects) should be specified.

Prediction of test results: All properties and circumstances that can influence the prediction of test results should be taken into account, including :

- geometrical parameters and their variability,
- geometrical imperfections,
- material properties,
- parameters influenced by fabrication and execution procedures,
- scale effects of environmental conditions taking into account, if relevant, any sequencing.

The expected modes of failure and/or calculation models, together with the corresponding variables should be described. If there is a significant doubt about which failure modes might be critical, then the test plan should be developed on the basis of accompanying pilot tests.

NOTE Attention needs to be given to the fact that a structural member can possess a number of fundamentally different failure modes.

Specification of test specimen and sampling: Test specimens should be specified, or obtained by sampling, in such a way as to represent the conditions of the real structure.

Factors to be taken into account include:

- dimensions and tolerances,
- material and fabrication of prototypes,
- number of test specimens,
- sampling procedures,
- restraints.

The objective of the sampling procedure should be to obtain a statistically representative sample.

Attention should be drawn to any difference between the test specimens and the product population that could influence the test results.

Loading specifications: The loading and environmental conditions to be specified for the test should include :

- loading points,
- loading history,
- restraints,
- temperatures,
- relative humidity,
- loading by deformation or force control, etc.

Load sequencing should be selected to represent the anticipated use of the structural member, under both normal and severe conditions of use. Interactions between the structural response and the apparatus used to apply the load should be taken into account where relevant.

Where structural behaviour depends upon the effects of one or more actions that will not be varied systematically, then those effects should be specified by their representative values.

Testing arrangement: The test equipment should be relevant for the type of tests and the expected range of measurements. Special attention should be given to measures to obtain sufficient strength and stiffness of the loading and supporting rigs, and clearance for deflections, etc.

Measurements : Prior to the testing, all relevant properties to be measured for each individual test specimen should be listed. Additionally a list should be made:

- a) of measurement-locations,
- b) of procedures for recording results, including if relevant :
 - time histories of displacements,
 - velocities,
 - accelerations,
 - strains,
 - forces and pressures,
 - required frequency,
 - accuracy of measurements, and
 - appropriate measuring devices.

Evaluation and reporting the test: For specific guidance, see D5 to D8. Any Standards on which the tests are based should be reported.

D5 Derivation of design values

(1) The derivation from tests of the design values for a material property, a model parameter or a resistance should be carried out in one of the following ways:

- a) by assessing a characteristic value, which is then divided by a partial factor and possibly multiplied if necessary by an explicit conversion factor (see D7.2 and D8.2) ;
- b) by direct determination of the design value, implicitly or explicitly accounting for the conversion of results and the total reliability required (see D7.3 and D8.3).

Note: In general method a) is to be preferred provided the value of the partial factor is determined from the normal design procedure (see (3) below).

(2) The derivation of a characteristic value from tests (Method (a)) should take into account:

- a) the scatter of test data ;
- b) statistical uncertainty associated with the number of tests ;
- c) prior statistical knowledge.

(3) The partial factor to be applied to a characteristic value should be taken from the appropriate ES provided there is sufficient similarity between the tests and the usual field of application of the partial factor as used in numerical verifications.

(4) If the response of the structure or structural member or the resistance of the material depends on influences not sufficiently covered by the tests such as:

- time and duration effects,
- scale and size effects,
- different environmental, loading and boundary conditions,
- resistance effects,

then the calculation model should take such influences into account as appropriate.

(5) In special cases where the method given in D5(1)b) is used, the following should be taken into account when determining design values :

- the relevant limit states ;
- the required level of reliability ;
- compatibility with the assumptions relevant to the actions side in expression (C.8a) ;
- where appropriate, the required design working life ;
- prior knowledge from similar cases.

Note: Further information may be found in D6, D7 and D8.

D6 General principles for statistical evaluations

(1) When evaluating test results, the behaviour of test specimens and failure modes should be compared with theoretical predictions. When significant deviations from a prediction occur, an explanation should be sought : this might involve additional testing, perhaps under different conditions, or modification of the theoretical model.

(2) The evaluation of test results should be based on statistical methods, with the use of available (statistical) information about the type of distribution to be used and its associated parameters. The methods given in this Annex may be used only when the following conditions are satisfied :

- the statistical data (including prior information) are taken from identified populations which are sufficiently homogeneous ; and
- a sufficient number of observations is available.

Note: At the level of interpretation of tests results, three main categories can be distinguished :

- where one test only (or very few tests) is (are) performed, no classical statistical interpretation is possible. Only the use of extensive prior information associated with hypotheses about the relative degrees of importance of this information and of the test results, make it possible to present an interpretation as
 - statistical (Bayesian procedures, see ES ISO 12491) ;
- if a larger series of tests is performed to evaluate a parameter, a classical statistical interpretation might be possible. The commoner cases are treated, as examples, in D7. This interpretation will still need to use some prior information about the parameter ; however, this will normally be less than above.
- when a series of tests is carried out in order to calibrate a model (as a function) and one or more associated parameters, a classical statistical interpretation is possible.

(3) The result of a test evaluation should be considered valid only for the specifications and load characteristics considered in the tests. If the results are to be extrapolated to cover other design parameters and loading, additional information from previous tests or from theoretical bases should be used.

D7 Statistical determination of a single property

D7.1 General

(1) This clause gives working expressions for deriving design values from test types (a) and (b) of D3(3) for a single property (for example, a strength) when using evaluation methods (a) and (b) of D5(1).

Note: The expressions presented here, which use Bayesian procedures with “vague” prior distributions, lead to almost the same results as classical statistics with confidence levels equal to 0.75.

(2) The single property X may represent

- a) a resistance of a product,
- b) a property contributing to the resistance of a product.

(3) In case a) the procedure D7.2 and D7.3 can be applied directly to determine characteristic or design or partial factor values.

(4) In case b) it should be considered that the design value of the resistance should also include:

- the effects of other properties,
- the model uncertainty,
- other effects (scaling, volume, etc.)

(5) The tables and expressions in D7.2 and D7.3 are based on the following assumptions:

- all variables follow either a Normal or a log-normal distribution ;
- there is no prior knowledge about the value of the mean ;
- for the case " V_X unknown", there is no prior knowledge about the coefficient of variation ;
- for the case " V_X known", there is full knowledge of the coefficient of variation.

Note: Adopting a log-normal distribution for certain variables has the advantage that no negative values can occur as for example for geometrical and resistance variables.

In practice, it is often preferable to use the case " V_X known" together with a conservative upper estimate of V_X , rather than to apply the rules given for the case " V_X unknown". Moreover V_X , when unknown, should be assumed to be not smaller than 0.10.

D7.2 Assessment via the characteristic value

(1) The design value of a property X should be found by using:

$$X_d = \eta_d \frac{X_{k(n)}}{\gamma_m} = \frac{\eta_d}{\gamma_m} m_X \{1 - k_n V_X\} \quad (\text{D.1})$$

where :

η_d is the design value of the conversion factor.

Note: The assessment of the relevant conversion factor is strongly dependent on the type of test and the type of material.

The value of k_n can be found from Table D1.

(2) When using table D1, one of two cases should be considered as follows.

- The row " V_X known" should be used if the coefficient of variation, V_X , or a realistic upper bound of it, is known from prior knowledge.

Note: Prior knowledge might come from the evaluation of previous tests in comparable situations. What is ‘comparable’ needs to be determined by engineering judgment (see D7.1(3)).

- The row " V_X unknown" should be used if the coefficient of variation V_X is not known from prior knowledge and so needs to be estimated from the sample as:

$$s_x^2 = \frac{1}{n-1} \sum (x_i - m_x)^2 \tag{D.2}$$

$$V_x = s_x / m_x \tag{D.3}$$

(3) The partial factor γ_m should be selected according to the field of application of the test results.

Table D1: Values of k_n for the 5% characteristic value

n	1	2	3	4	5	6	8	10	20	30	∞
V_x known	2.31	2.01	1.89	1.83	1.80	1.77	1.74	1.72	1.68	1.67	1.64
V_x unknown	-	-	3.37	2.63	2.33	2.18	2.00	1.92	1.76	1.73	1.64

Note 1: This table is based on the Normal distribution.

Note 2: With a log-normal distribution expression (D.1) becomes:

$$X_d = \frac{\eta_d}{\gamma_m} \exp[m_y - k_n s_y]$$

where :

$$m_y = \frac{1}{n} \sum \ln(x_i)$$

If V_X is known from prior knowledge, $s_y = \sqrt{\ln(V_X^2 + 1)} \approx V_X$

If V_X is unknown from prior knowledge, $s_y = \sqrt{\frac{1}{n-1} \sum (\ln x_i - m_y)^2}$

D7.3 Direct assessment of the design value for ULS verifications

- (1) The design value X_d for X should be found by using:

$$X_d = \eta_d m_x \{1 - k_{d,n} V_x\} \tag{D.4}$$

In this case, η_d should cover all uncertainties not covered by the tests.

- (2) $k_{d,n}$ should be obtained from table D2.

Table D2 - Values of $k_{d,n}$ for the ULS design value.

n	1	2	3	4	5	6	8	10	20	30	∞
V_x known	4.36	3.77	3.56	3.44	3.37	3.33	3.27	3.23	3.16	3.13	3.04
V_x unknown	-	-	-	11.40	7.85	6.36	5.07	4.51	3.64	3.44	3.04

Note 1: This table is based on the assumption that the design value corresponds to a product $\alpha_R \beta = 0.8 \times 3.8 = 3.04$ (see annex C) and that X is Normally distributed. This gives a probability of observing a lower value of about 0.1 %.

Note 2: With a log-normal distribution, expression (D.4) becomes:

$$X_d = \eta_d \exp \left[m_y - k_{d,n} s_y \right]$$

D8 Statistical determination of resistance models

D8.1 General

(1) This clause is mainly intended to define procedures (methods) for calibrating resistance models and for deriving design values from tests type d) (see D3(1)). Use will be made of available prior information (knowledge or assumptions).

(2) Based on the observation of actual behaviour in tests and on theoretical considerations, a “design model” should be developed, leading to the derivation of a resistance function. The validity of this model should be then checked by means of a statistical interpretation of all available test data. If necessary the design model is then adjusted until sufficient correlation is achieved between the theoretical values and the test data.

(3) Deviation in the predictions obtained by using the design model should also be determined from the tests. This deviation will need to be combined with the deviations of the other variables in the resistance function in order to obtain an overall indication of deviation. These other variables include :

- deviation in material strength and stiffness ;
- deviation in geometrical properties.

(4) The characteristic resistance should be determined by taking account of the deviations of all the variables.

(5) In D5(1) two different methods are distinguished. These methods are given in D8.2 and D8.3 respectively. Additionally, some possible simplifications are given in D8.4.

These methods are presented as a number of discrete steps and some assumptions regarding the test population are made and explained; these assumptions are to be considered to be no more than recommendations covering some of the commoner cases.

D8.2 Standard evaluation procedure (Method (a))

D8.2.1 General

- (1) For the standard evaluation procedure the following assumptions are made:
- a) the resistance function is a function of a number of independent variables \underline{X} ;
 - b) a sufficient number of test results is available;
 - c) all relevant geometrical and material properties are measured;
 - d) there is no correlation (statistical dependence) between the variables in the resistance function;
 - e) all variables follow either a Normal or a log-normal distribution.

Note: Adopting a log-normal distribution for a variable has the advantage that no negative values can occur.

(2) The standard procedure for method D5(1)a comprises the seven steps given in D8.2.2.1 to D8.2.2.7.

D8.2.2 Standard procedure

D8.2.2.1 Step 1 : Develop a design model

(1) Develop a design model for the theoretical resistance r_t of the member or structural detail considered, represented by the resistance function :

$$r_t = g_r(\underline{X}) \quad (\text{D.5})$$

(2) The resistance function should cover all relevant basic variables \underline{X} that affect the resistance at the relevant limit state.

(3) All basic parameters should be measured for each test specimen i (assumption (c) in D8.2.1) and should be available for use in the evaluation.

D8.2.2.2 Step 2: Compare experimental and theoretical values

(1) Substitute the actual measured properties into the resistance function so as to obtain theoretical values r_{ti} to form the basis of a comparison with the experimental values r_{ei} from the tests.

(2) The points representing pairs of corresponding values (r_{ti} , r_{ei}) should be plotted on a diagram, as indicated in figure D1.

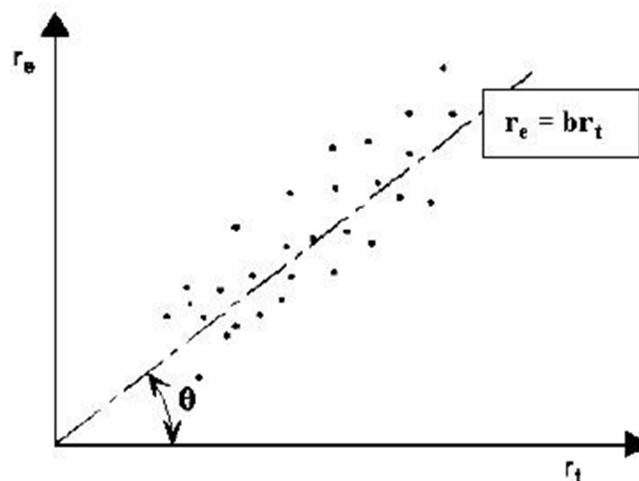


Figure D1 - r_e - r_t diagram

(3) If the resistance function is exact and complete, then all of the points will lie on the line $\theta = \pi/4$. In practice the points will show some scatter, but the causes of any systematic deviation from that line should be investigated to check whether this indicates errors in the test procedures or in the resistance function.

D8.2.2.3 Step 3: Estimate the mean value correction factor b

(1) Represent the probabilistic model of the resistance r in the format:

$$r = br_i\delta \quad (D.6)$$

where:

b is the “Least Squares” best-fit to the slope, given by $b = \frac{\sum r_e r_t}{\sum r_t^2}$ (D.7)

(2) The mean value of the theoretical resistance function, calculated using the mean values \underline{X}_m of the basic variables, can be obtained from:

$$r_m = br_t(\underline{X}_m)\delta = bg_{rt}(\underline{X}_m)\delta \quad (D.8)$$

D8.2.2.4 Step 4: Estimate the coefficient of variation of the errors

(1) The error term δ_i for each experimental value r_{ei} should be determined from expression (D.9):

$$\delta_i = \frac{r_{ei}}{br_{ti}} \quad (D.9)$$

(2) From the values of δ_i an estimated value for V_δ should be determined by defining:

$$\Delta_i = \ln(\delta_i) \quad (D.10)$$

(3) The estimated value $\bar{\Delta}$ for $E(\Delta)$ should be obtained from:

$$\bar{\Delta} = \frac{1}{n} \sum_{i=1}^n \Delta_i \quad (D.11)$$

(4) The estimated value s_Δ^2 for σ_Δ^2 should be obtained from:

$$s_\Delta^2 = \frac{1}{n-1} \sum_{i=1}^n (\Delta_i - \bar{\Delta})^2 \quad (D.12)$$

(5) The expression:

$$V_\delta = \sqrt{\exp(s_\Delta^2) - 1} \quad (D.13)$$

may be used as the coefficient of variation V_δ of the δ_i error terms.

D8.2.2.5 Step 5: Analyze compatibility

(1) The compatibility of the test population with the assumptions made in the resistance function should be analyzed.

(2) If the scatter of the (r_{ei}, r_{ii}) values is too high to give economical design resistance functions, this scatter may be reduced in one of the following ways:

- a) by correcting the design model to take into account parameters which had previously been ignored;
- b) by modifying b and V_δ by dividing the total test population into appropriate sub-sets for which the influence of such additional parameters may be considered to be constant.

(3) To determine which parameters have most influence on the scatter, the test results may be split into subsets with respect to these parameters.

Note: The purpose is to improve the resistance function per sub-set by analyzing each subset using the standard procedure. The disadvantage of splitting the test results into sub-sets is that the number of test results in each sub-set can become very small.

(4) When determining the fractile factors k_n (see step 7), the k_n value for the sub-sets may be determined on the basis of the total number of the tests in the original series.

Note: Attention is drawn to the fact that the frequency distribution for resistance can be better described by a bi-modal or a multi-modal function. Special approximation techniques can be used to transform these functions into a uni-modal distribution.

D8.2.2.6 Step 6: Determine the coefficients of variation V_{X_i} of the basic variables

(1) If it can be shown that the test population is fully representative of the variation in reality, then the coefficients of variation V_{X_i} of the basic variables in the resistance function may be determined from the test data. However, since this is not generally the case, the coefficients of variation V_{X_i} will normally need to be determined on the basis of some prior knowledge.

D8.2.2.7 Step 7: Determine the characteristic value r_k of the resistance

(1) If the resistance function for j basic variables is a product function of the form:

$$r = br_i \delta = b \{X_1 \times X_2 \dots X_j\} \delta$$

the mean value $E(r)$ may be obtained from :

$$E(r) = b \{E(X_1) \times E(X_2) \dots E(X_i)\} = bg_{r_i}(\underline{X}_m) \quad (\text{D.14a})$$

and the coefficient of variation V_r may be obtained from the product function :

$$V_r^2 = (V_\delta^2 + 1) \left[\prod_{i=1}^j (V_{X_i}^2 + 1) \right] - 1 \quad (D.14b)$$

(2) Alternatively, for small values of V_δ^2 and $V_{X_i}^2$ the following approximation for V_r may be used:

$$V_r^2 = V_\delta^2 + V_{rt}^2 \quad (D.15a)$$

with:

$$V_{rt}^2 = \sum_{i=1}^j V_{X_i}^2 \quad (D.15b)$$

(3) If the resistance function is a more complex function of the form:

$$r = br_i \delta = bg_{rt}(X_1, \dots, X_j) \delta$$

the mean value $E(r)$ may be obtained from:

$$E(r) = bg_{rt}(E(X_1), \dots, E(X_j)) = bg_{rt}(X_m) \quad (D.16a)$$

and the coefficient of variation V_{rt} may be obtained from :

$$V_{rt}^2 = \frac{VAR[g_{rt}(X)]}{g_{rt}^2(X_m)} \cong \frac{1}{g_{rt}^2(X_m)} \times \sum_{i=1}^j \left(\frac{\partial g_{rt}}{\partial X_i} \sigma_i \right)^2 \quad (D.16b)$$

(4) If the number of tests is limited (say $n < 100$) allowance should be made in the distribution of Δ for statistical uncertainties. The distribution should be considered as a central t-distribution with the parameters $\bar{\Delta}$, V_Δ and n .

(5) In this case the characteristic resistance r_k should be obtained from:

$$r_k = bg_{rt}(X_m) \exp(-k_\infty \alpha_{rt} Q_{rt} - k_n \alpha_\delta Q_\delta - 0.5Q^2) \quad (D.17)$$

with :

$$Q_{rt} = \sigma_{\ln(r)} = \sqrt{\ln(V_{rt}^2 + 1)} \quad (D.18a)$$

$$Q_\delta = \sigma_{\ln(\delta)} = \sqrt{\ln(V_\delta^2 + 1)} \quad (D.18b)$$

$$Q_\delta = \sigma_{\ln(r)} = \sqrt{\ln(V_r^2 + 1)} \quad (D.18c)$$

$$\alpha_{rt} = \frac{Q_{rt}}{Q} \quad (D.19a)$$

$$\alpha_{\delta} = \frac{Q_{\delta}}{Q} \quad (\text{D.19b})$$

where :

k_n is the characteristic fractile factor from table D1 for the case V_X unknown ;

k_{∞} is the value of k_n for $n \rightarrow \infty$ [$k_{\infty} = 1.64$];

α_{rt} is the weighting factor for Q_{rt}

α_{δ} is the weighting factor for Q_{δ}

Note: The value of V_{δ} is to be estimated from the test sample under consideration.

(6) If a large number of tests ($n \geq 100$) is available, the characteristic resistance r_k may be obtained from:

$$r_k = bg_{rt}(\underline{X}_m) \exp(-k_{\infty}Q - 0.5Q^2) \quad (\text{D.20})$$

D8.3 Standard evaluation procedure (Method (b))

(1) In this case the procedure is the same as in D8.2, excepted that step 7 is adapted by replacing the characteristic fractile factor k_n by the design fractile factor $k_{d,n}$ equal to the product $\alpha_R \beta$ assessed at $0.8 \times 3.8 = 3.04$ as commonly accepted (see Annex C) to obtain the design value r_d of the resistance.

(2) For the case of a limited number of tests the design value r_d should be obtained from:

$$r_d = bg_{rt}(\underline{X}_m) \exp(-k_{d,\infty} \alpha_{rt} Q_{rt} - k_{d,n} \alpha_{\delta} Q_{\delta} - 0.5Q^2) \quad (\text{D.21})$$

where :

$k_{d,n}$ is the design fractile factor from table D2 for the case “ V_X unknown” ;

$k_{d,\infty}$ is the value of $k_{d,n}$ for $n \rightarrow \infty$ [$k_{d,\infty} = 3.04$]

Note: The value of V_{δ} is to be estimated from the test sample under consideration

(2) For the case of a large number of tests the design value r_d may be obtained from:

$$r_d = bg_{rt}(\underline{X}_m) \exp(-k_{d,\infty}Q - 0.5Q^2) \quad (\text{D.22})$$

D8.4 Use of additional prior knowledge

(1) If the validity of the resistance function r_t and an upper bound (conservative estimate) for the coefficient of variation V_r are already known from a significant number of previous tests, the following simplified procedure may be adopted when further tests are carried out.

(2) If only one further test is carried out, the characteristic value r_k may be determined from the result r_e of this test by applying:

$$r_k = \eta_k r_e \quad (\text{D.23})$$

where :

η_k is a reduction factor applicable in the case of prior knowledge that may be obtained from:

$$\eta_k = 0.9 \exp(-2.31V_r - 0.5V_r^2) \quad (\text{D.24})$$

where :

V_r is the maximum coefficient of variation observed in previous tests.

(3) If two or three further tests are carried out, the characteristic value r_k may be determined from the mean value r_{em} of the test results by applying:

$$r_k = \eta_k r_{em} \quad (\text{D.25})$$

where:

η_k is a reduction factor applicable in the case of prior knowledge that may be obtained from:

$$\eta_k = \exp(-2.0V_r - 0.5V_r^2) \quad (\text{D.26})$$

where :

V_r is the maximum coefficient of variation observed in previous tests.

provided that each extreme (maximum or minimum) value r_{ee} satisfies the condition:

$$|r_{ee} - r_{em}| \leq 0.10r_{em} \quad (\text{D.27})$$

(4) The values of the coefficient of variation V_r given in table D3 may be assumed for the types of failure to be specified (e.g. in the relevant design code), leading to the listed values of η_k according to expressions (D.24) and (D.26).

Table D3 - Reduction factor η_k

Coefficient of variation V_r	Reduction factor η_k	
	For 1 test	For 2 or 3 tests
0.05	0.80	0.90
0.11	0.70	0.80
0.17	0.60	0.70

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- ES ISO 8930 General principles on reliability for structures - List of equivalent terms
- ES ISO 9001:2000 Quality management systems – Requirements
- ES ISO 10137 Basis for design of structures – Serviceability of buildings against vibrations
- ES ISO 8402 Quality management and quality assurance – Vocabulary



Organization and Objectives

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- ❖ Develop Ethiopian standards and establish a system that enable to check whether goods and services are in compliance with the required standards,
- ❖ Facilitate the country's technology transfer through the use of standards,
- ❖ Develop national standards for local products and services so as to make them competitive in the international market.

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